



NASA-DoD Lead-Free Electronics Project

DoD Soldering Technologies Working Group (STWG)

August 24 - 25, 2010

Resources

Project documents, test plans, test reports and other associated information will be available on the web:

- NASA-DoD Lead-Free Electronics Project:

http://www.teerm.nasa.gov/projects/NASA_DODLeadFreeElectronics_Proj2.html

- Joint Test Protocol
- Project Plan
- Test Reports

Project Stakeholders



U.S. AIR FORCE



**Rockwell
Collins**

BAE SYSTEMS



CELESTICA

calce™



NIHON SUPERIOR



Honeywell

COM DEV



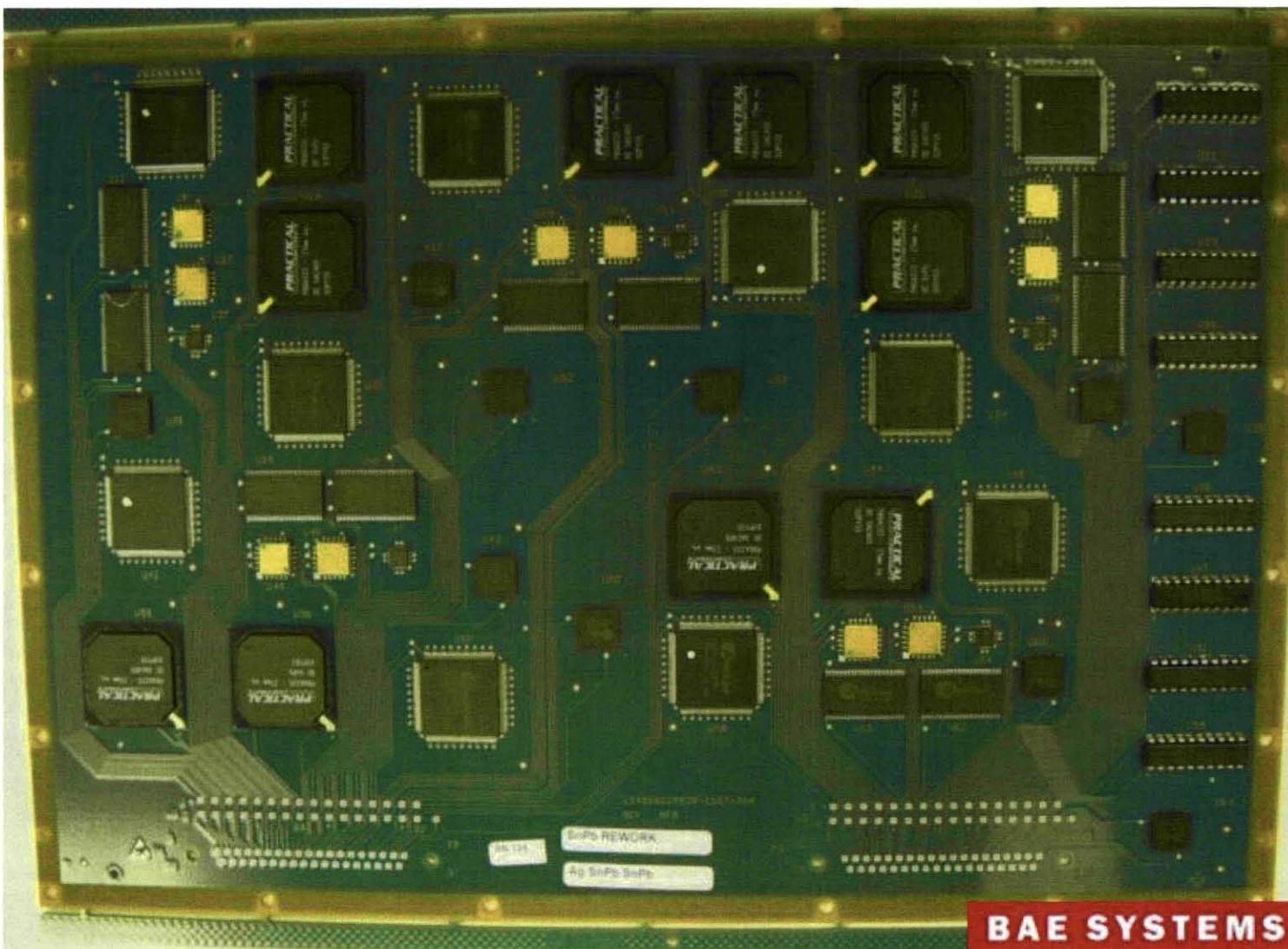
Raytheon

GENERAL DYNAMICS
Advanced Information Systems



Test Vehicles

- 193 Test Vehicles Assembled by BAE Systems (Irving, Texas)
120 = "Manufactured"
73 = "Rework"



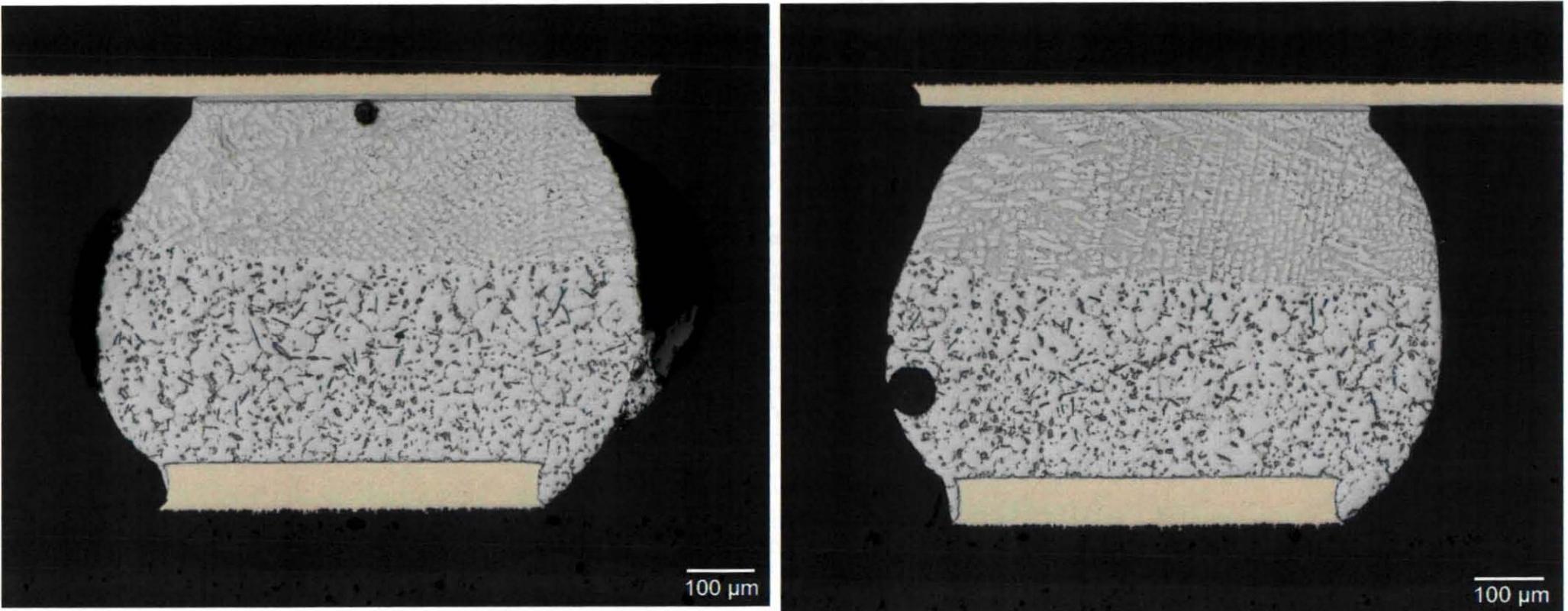
Circuit Cards

- 14.5"X 9"X 0.09"
- 6 layers of 0.5 ounce copper
- FR4 per IPC-4101/26 with a minimum Tg of 170°C (Isola 370HR)
- Pho-Tronics

Test Vehicle Characterization

Board # 3 SnPb As Fabricated
U18-BGA-225

Component Finish: SAC405, Reflow: SnPb



Reflow Soldering
Location – BAE Systems Irving, Texas
Reflow Profile = SnPb

- Preheat = ~ 120 seconds @ 140-183°C
- Solder joint peak temperature = 225°C
- Time above reflow = 60-90 sec
- Ramp Rate = 2-3 °C/sec

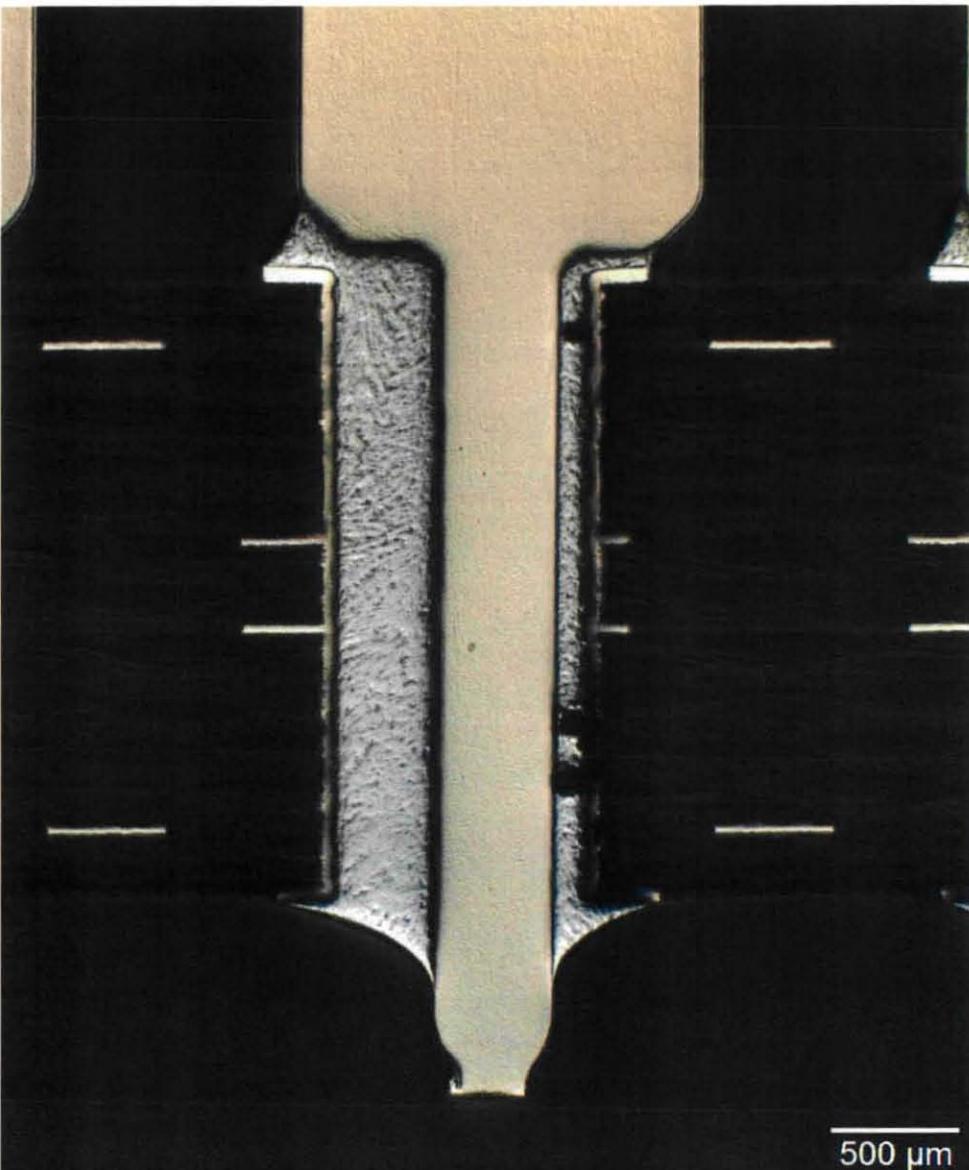


Test Vehicle Characterization

Board # 3 SnPb As Fabricated

U51-2 PDIP-20

Component Finish: Sn, Wave: SnPb

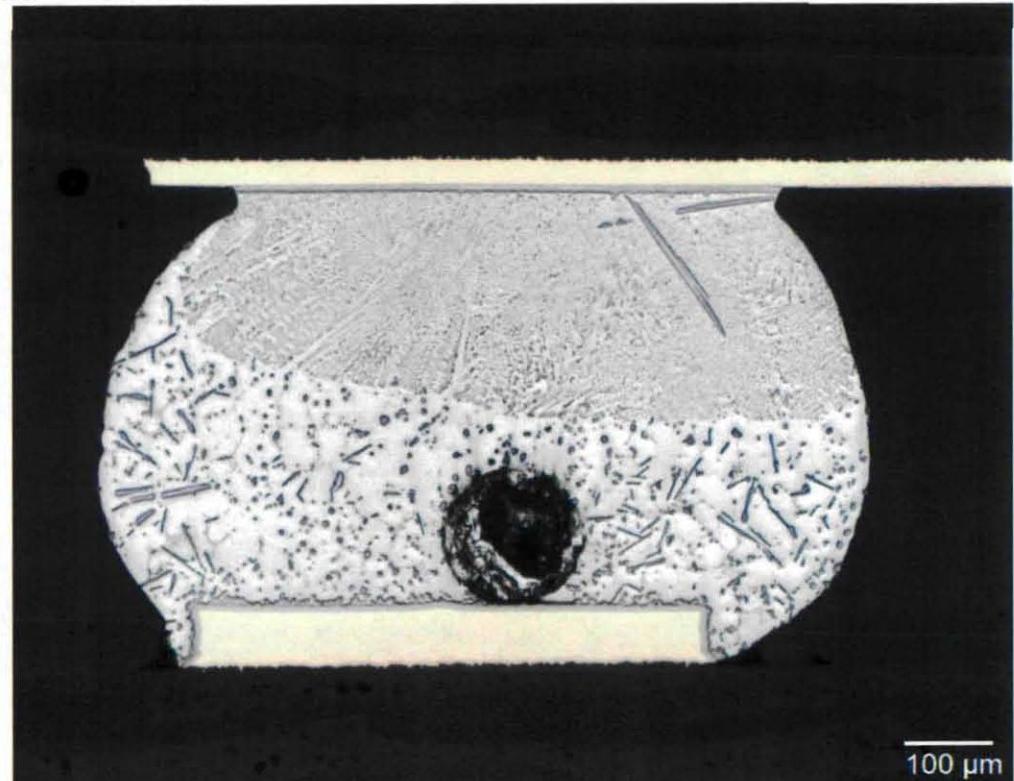
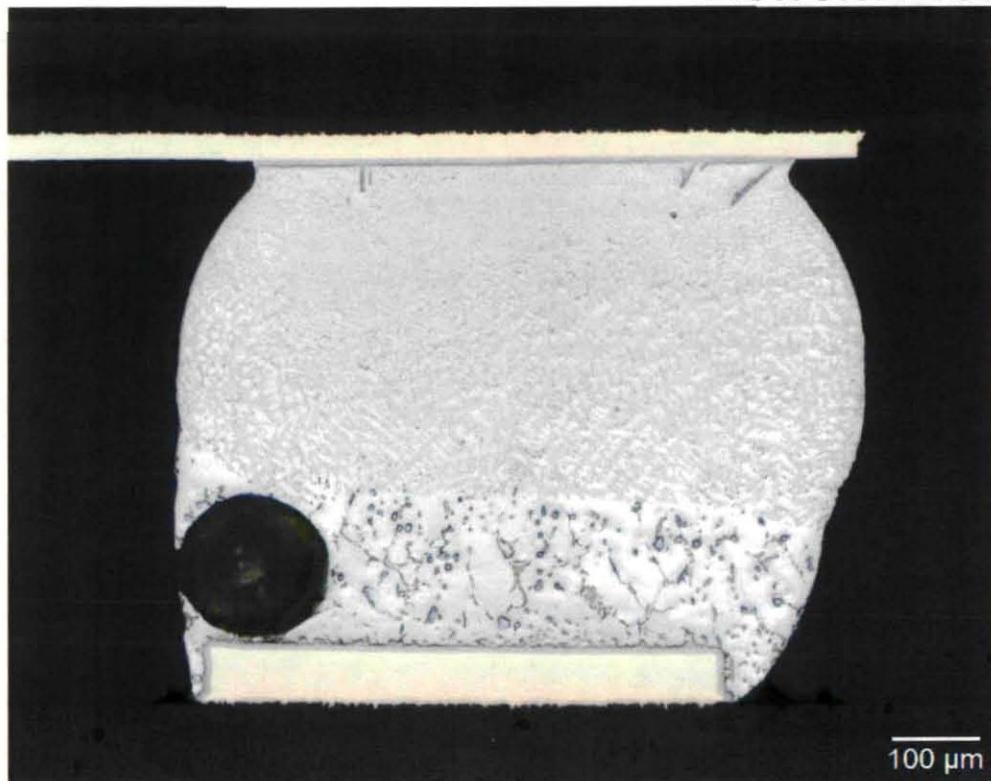


500 μm

Test Vehicle Characterization

Board # 154 SnPb Rework
U18 BGA-225

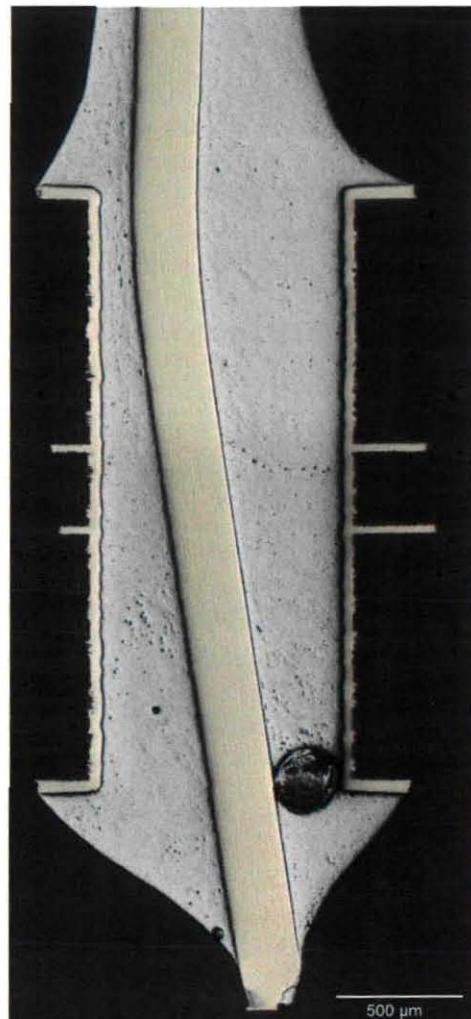
As assembled - Component Finish: SnPb, Reflow: SnPb
Reworked - Component Finish: SAC405, Rework Solder: SnPb
Rework Profile - SnPb



Test Vehicle Characterization

Board # 154 SnPb Rework
U51-1 PDIP-20

Component Finish: SnPb, Wave: SnPb
Reworked - Component Finish: Sn, Rework Solder: SnPb
Rework Profile - SnPb

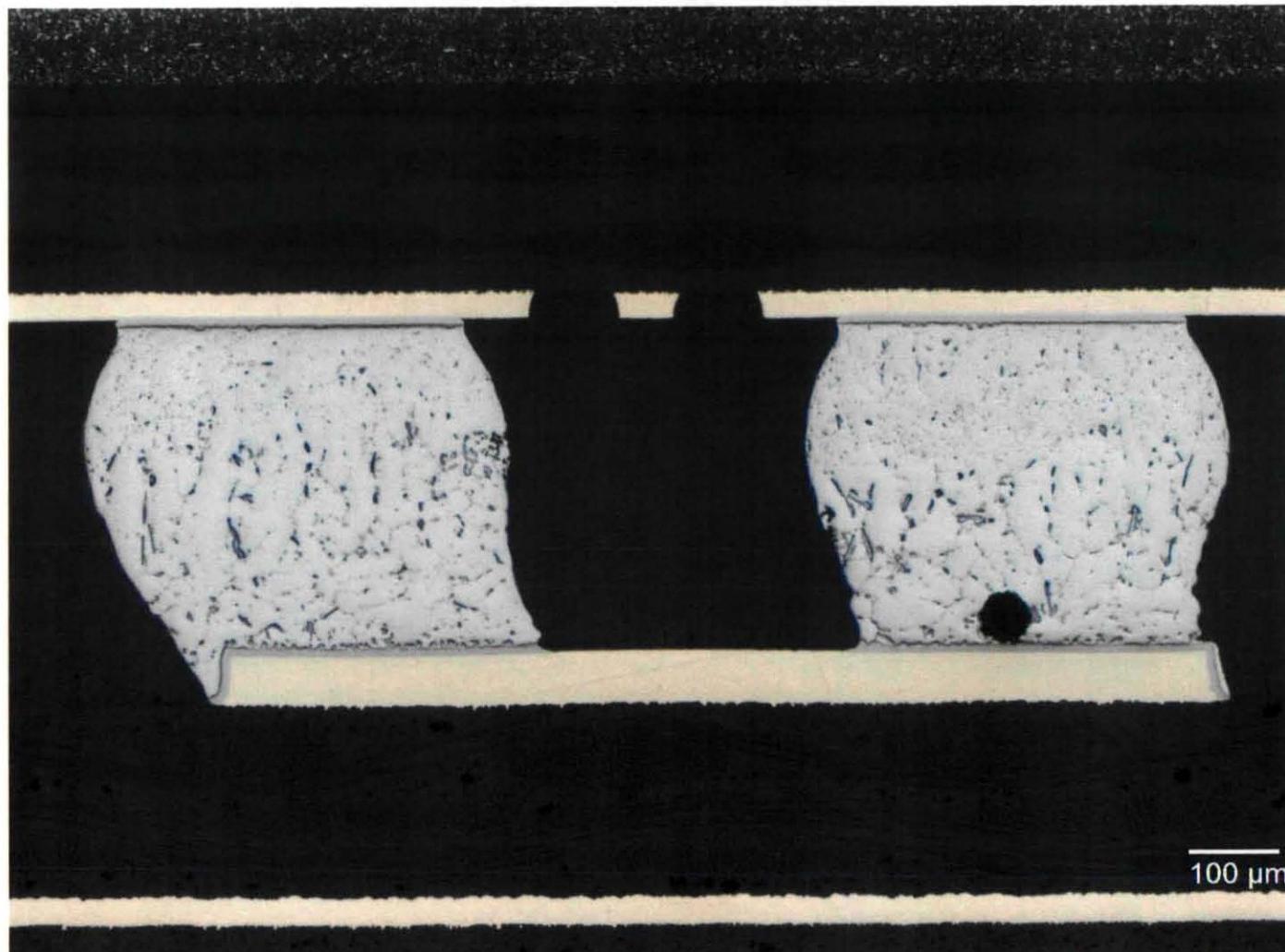


Test Vehicle Characterization

Board # 154 SnPb Rework
U60 CSP-100

Component Finish: SnPb , Reflow: SnPb

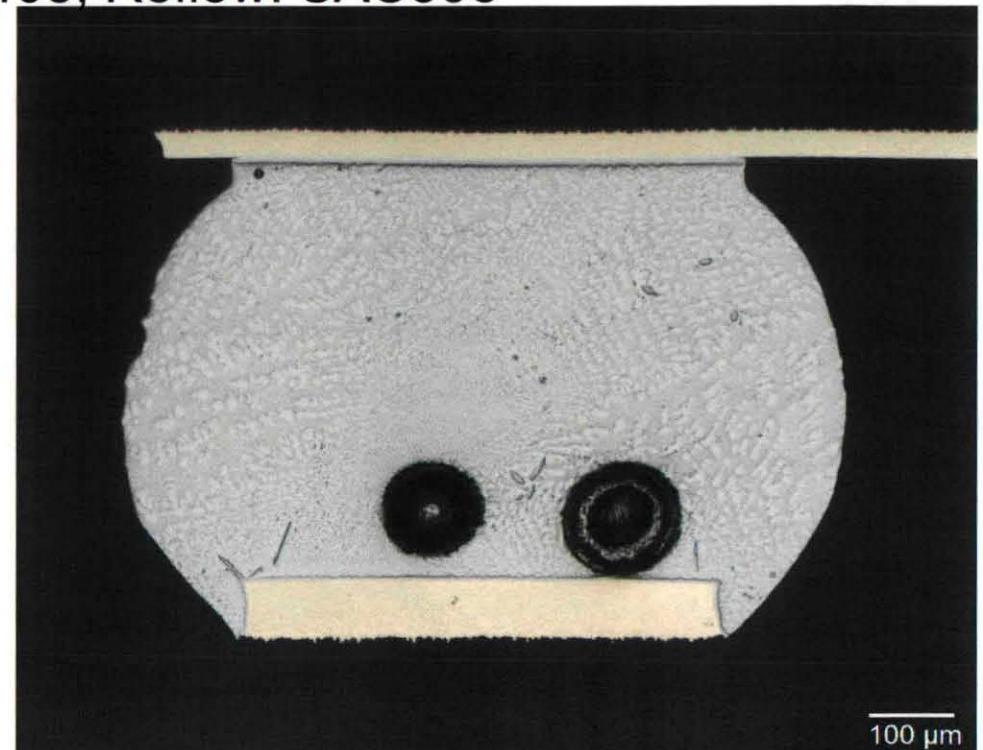
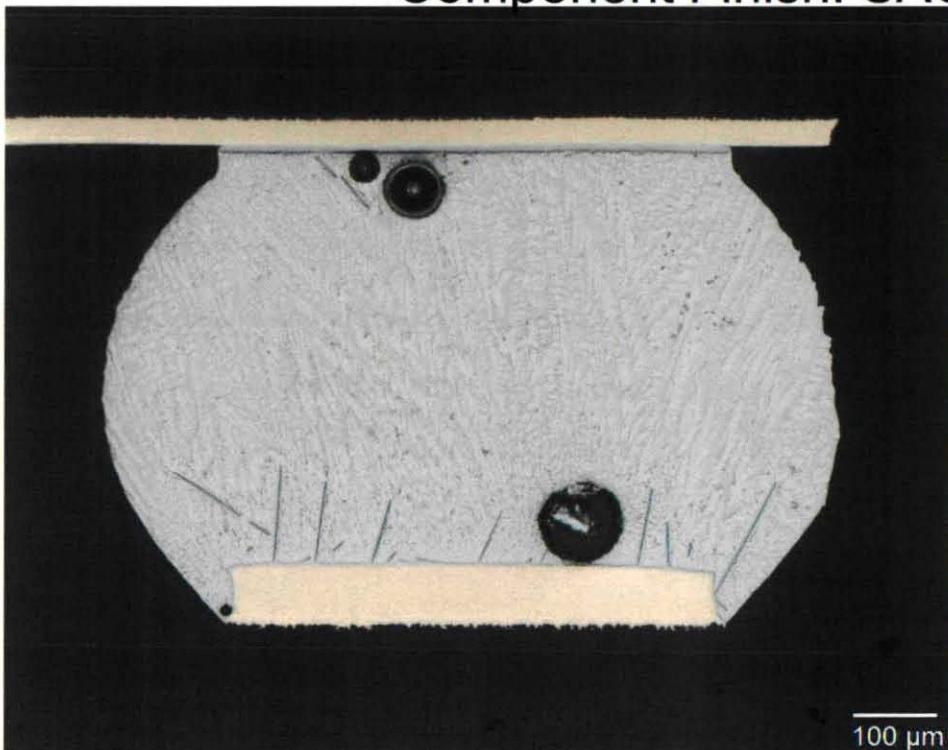
Reworked - Component Finish: SAC105, Rework Solder: SnPb
Rework Profile - SnPb



Test Vehicle Characterization

Board # 39 Lead Free As Fabricated
U2 BGA-225

Component Finish: SAC405, Reflow: SAC305



Reflow Soldering
Location – BAE Systems Irving, Texas

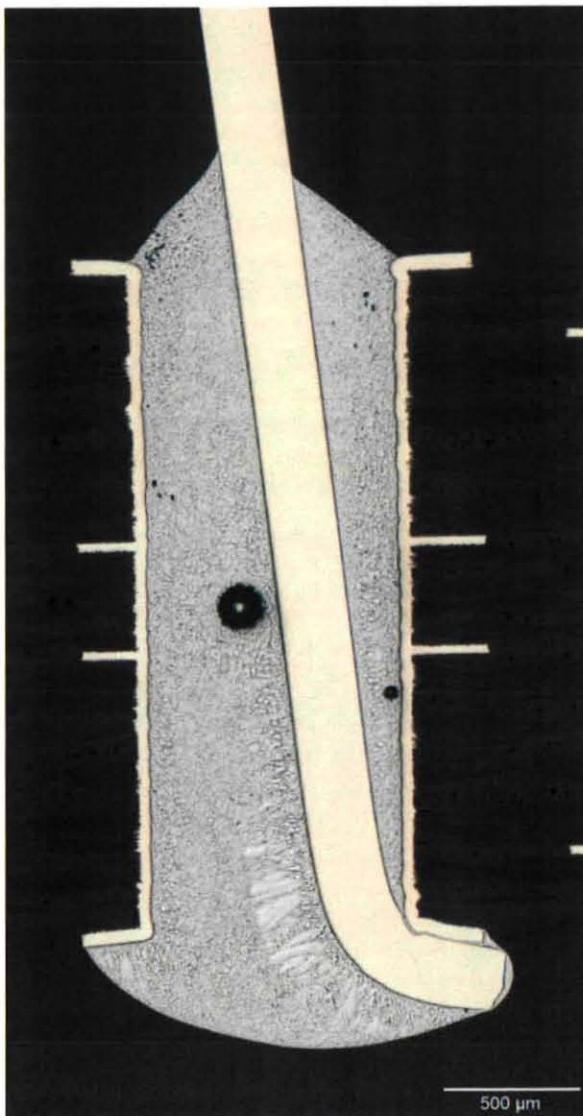
Reflow Profile = SAC305

- Preheat = 60-120 seconds @150-190°C
- Peak temperature target = 243°C
- Reflow: ~20 seconds above 230°C
- ~30-40 seconds above 220°C

Test Vehicle Characterization

Board # 39 Lead Free As Fabricated
U51-1 PDIP-20

Component Finish: NiPdAu, Wave: SN100C



NAVSEA Crane Rework Effort

Built 30 test vehicles (sub-set of the 193 assembled)

- Test vehicles were built with Lead-Free solder and Lead-Free component finishes only = similar to Manufactured test vehicles for Mechanical Shock, Vibration and Drop Testing
 - Lead-Free alloys, SAC305 and SN100C
 - Rework was done using only SnPb solder
 - Performed multiple pass rework 1 to 2 times on random Pb-free DIP, TQFP-144, TSOP-50, LCC and QFN components
 - Testing

**Rockwell
Collins**

COMPLETE

- Thermal Cycling -55°C to +125°C
 - Vibration Testing  CELESTICA. **COMPLETE**
 - Drop Testing  CELESTICA. **COMPLETE**

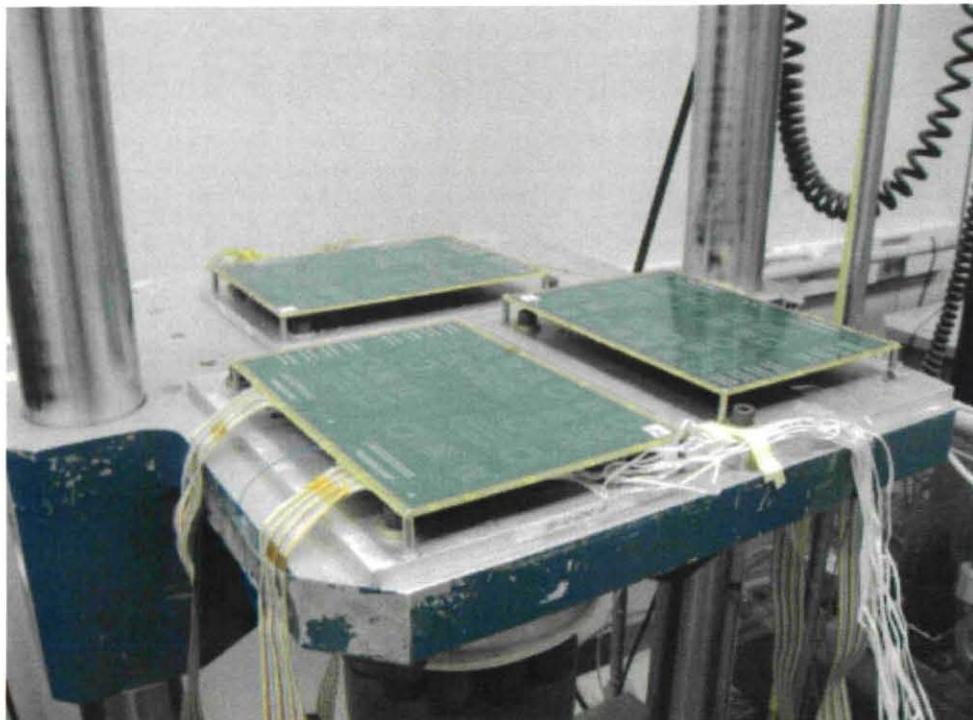
http://teerm.nasa.gov/NASA_DODLeadFreeElectronics_Proj2.html

Drop Testing



NSWC Crane Test Vehicles

- Shock parameters: 500 G, 2.0 ms duration (340 G for cards 80, 82, 87 for first)
- 10 drops)
- Number of drops: 20
- 9 cards in total / 3 cards tested per drop
- Each card monitored for shock response
- Each card monitored for resistance
- Cards 80, 83, 86 monitored for strain

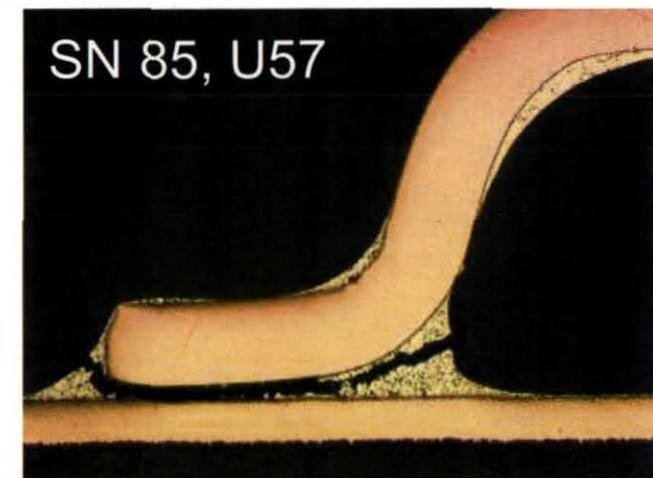


Drop Testing

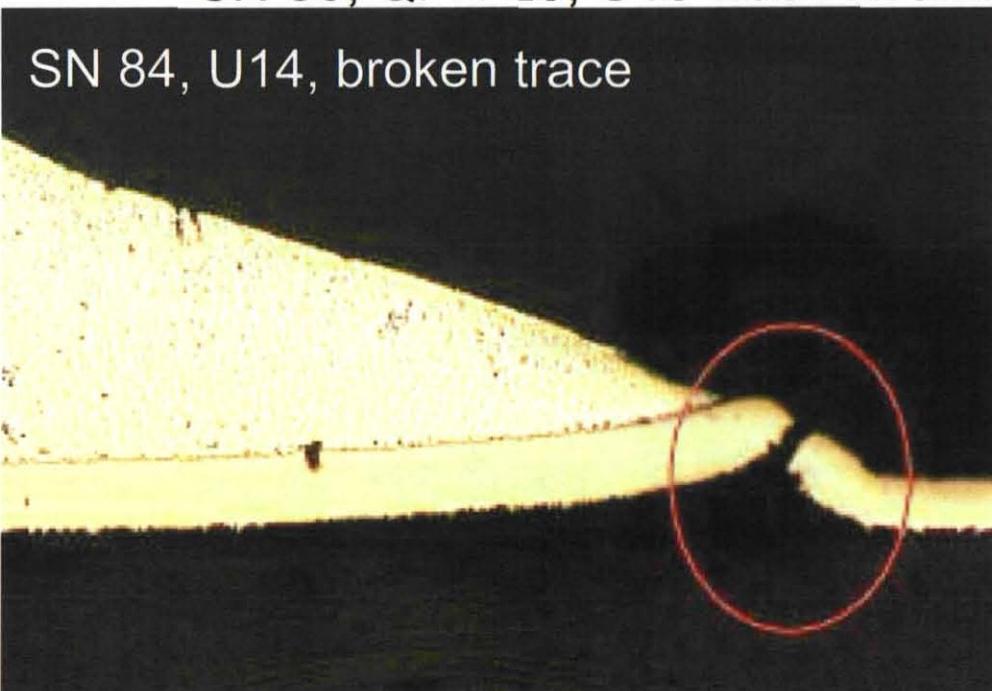


NSWC Crane Test Vehicles

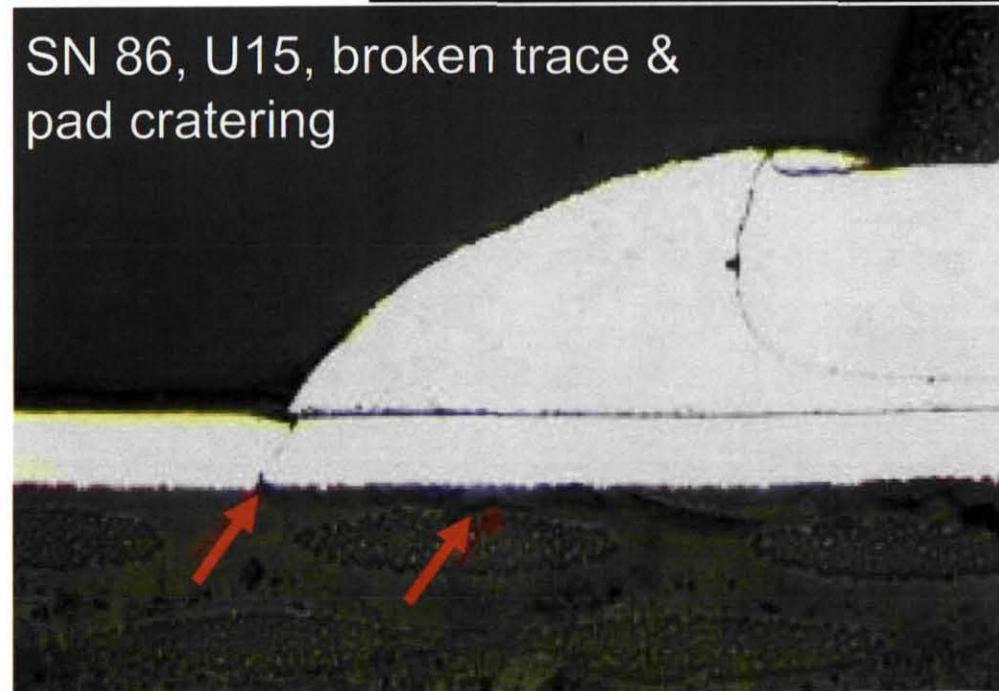
- Only component to have significant failures – BGA 225
- The 4 non-BGA samples that had an electrical failure had the following rework histories:
 - SN 85, TQFP 144, U57 was reworked once
 - SN 85, PDIP-20, U8 was reworked once
 - SN 84, CLCC-20, U14 was not reworked
 - SN 86, QFN-20, U15 was reworked twice



SN 84, U14, broken trace



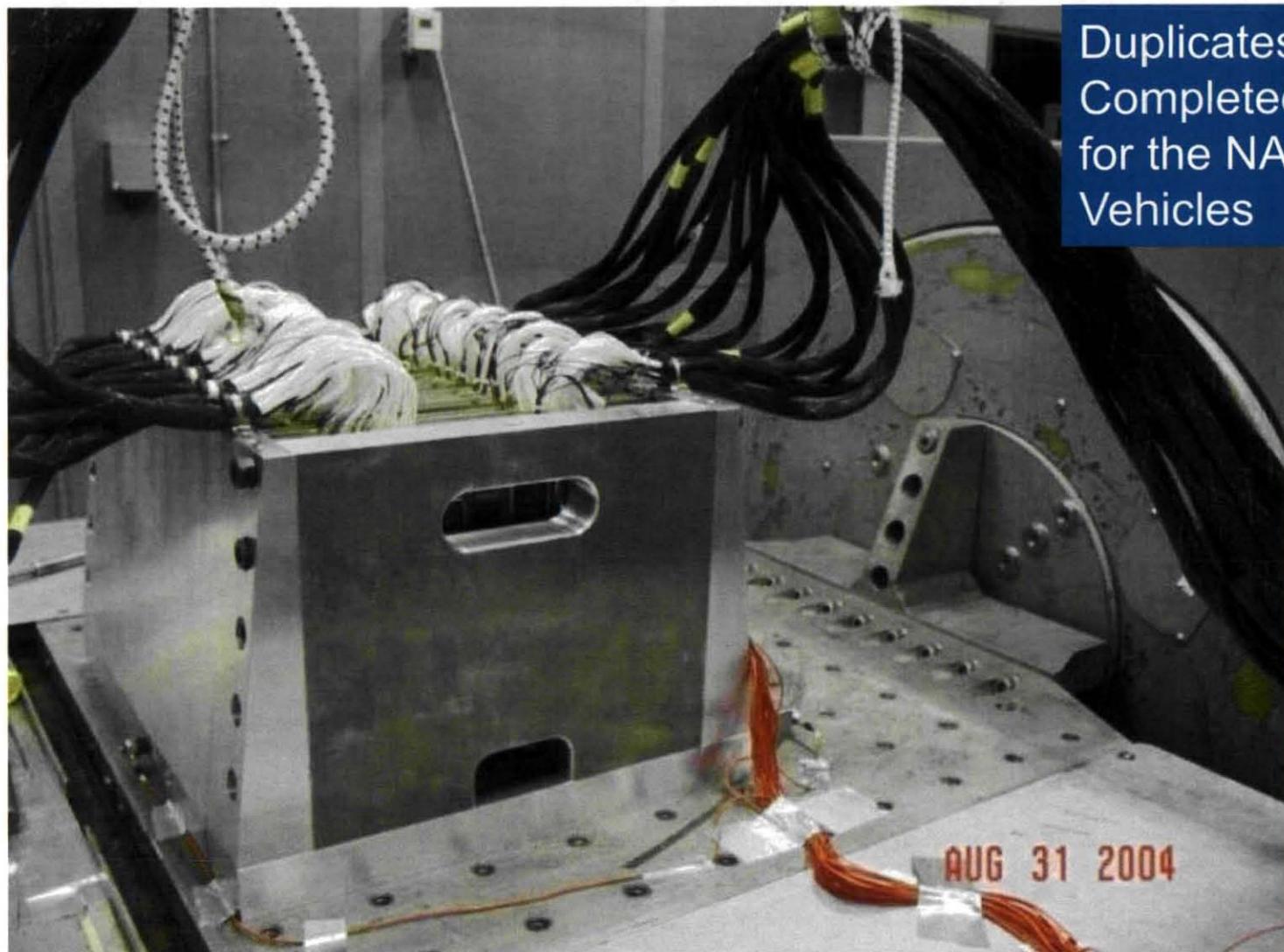
SN 86, U15, broken trace & pad cratering



Vibration Testing



Subject the test vehicles to 8.0 g_{rms} for one hour. Then increase the Z-axis vibration level in 2.0 g_{rms} increments, shaking for one hour per step until the 20.0 g_{rms} level is completed. Then subject the test vehicles to a final one hour of vibration at 28.0 g_{rms}.



Duplicates Testing
Completed by Boeing
for the NASA-DoD Test
Vehicles

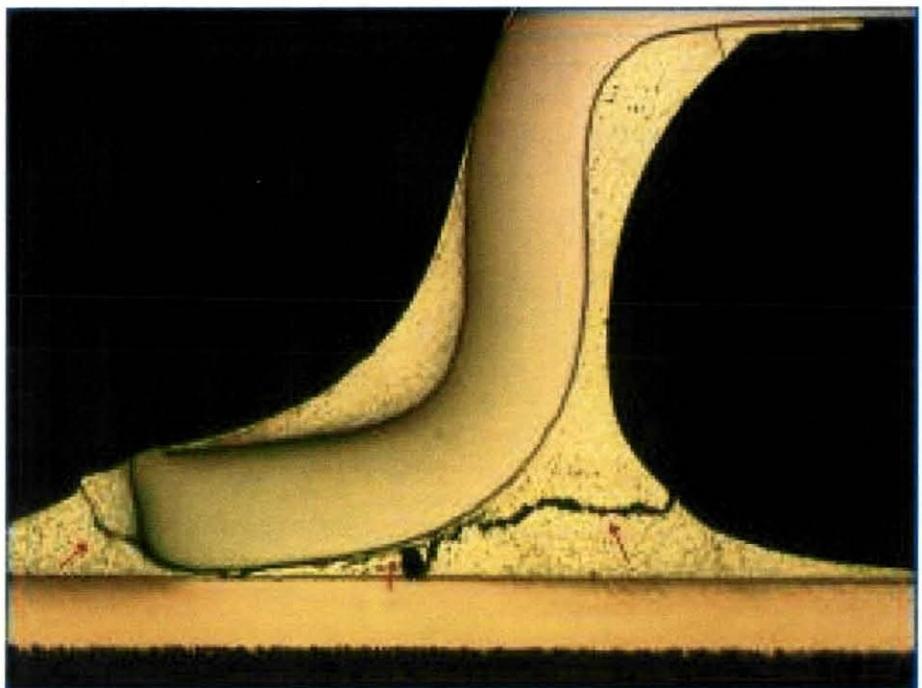
Vibration Testing



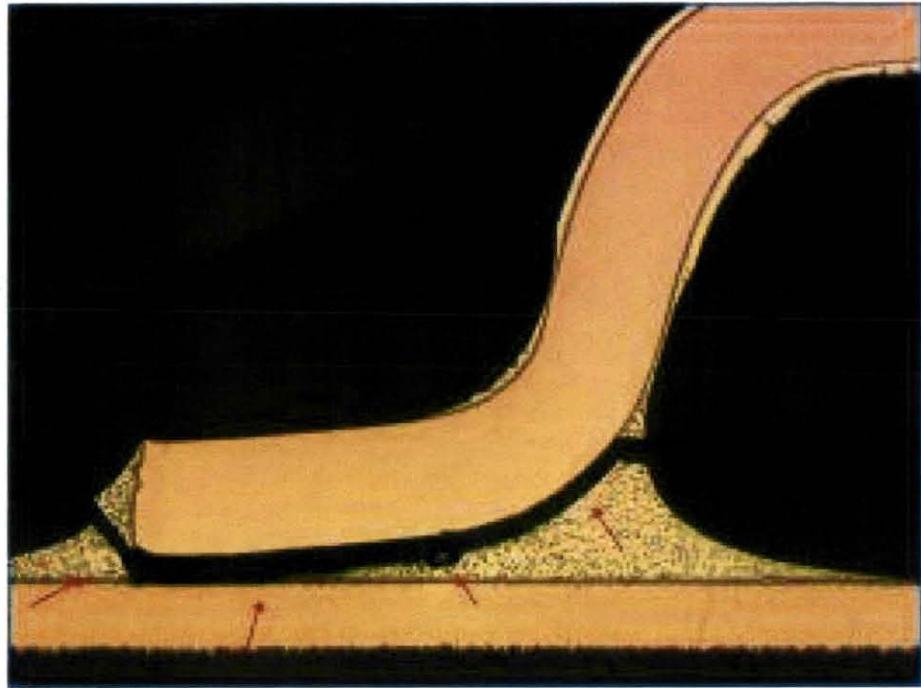
- Among the parameters tested, unexplained variation continues to dominate the results
 - Batch or Card S/N did not significantly influence the results
 - Component package style had a marked influence on both the time to failure (T_f) and on the number of cycles to 10% failure (N₁₀)
- Rework
 - Did influence time to failure
 - Did not significantly influence N₁₀
- Location on the board
 - Did significantly influence time to failure
 - Did not significantly influence N₁₀

Vibration Testing

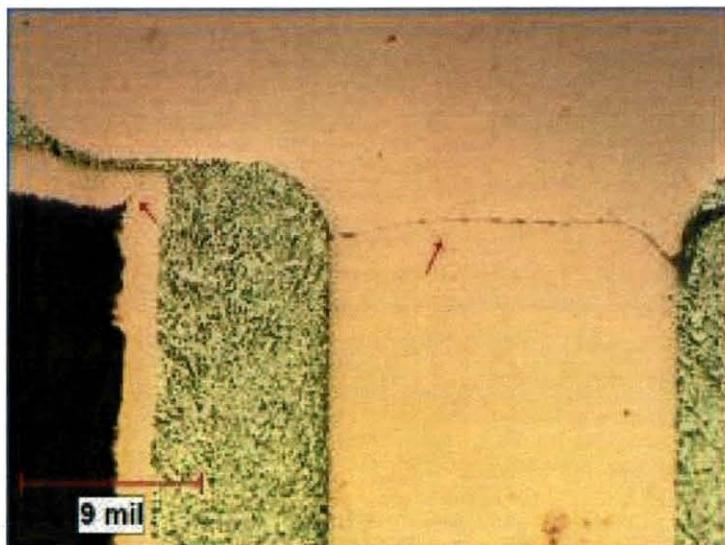
 CELESTICA.



SN67, U61, left lead solder crack, 100x

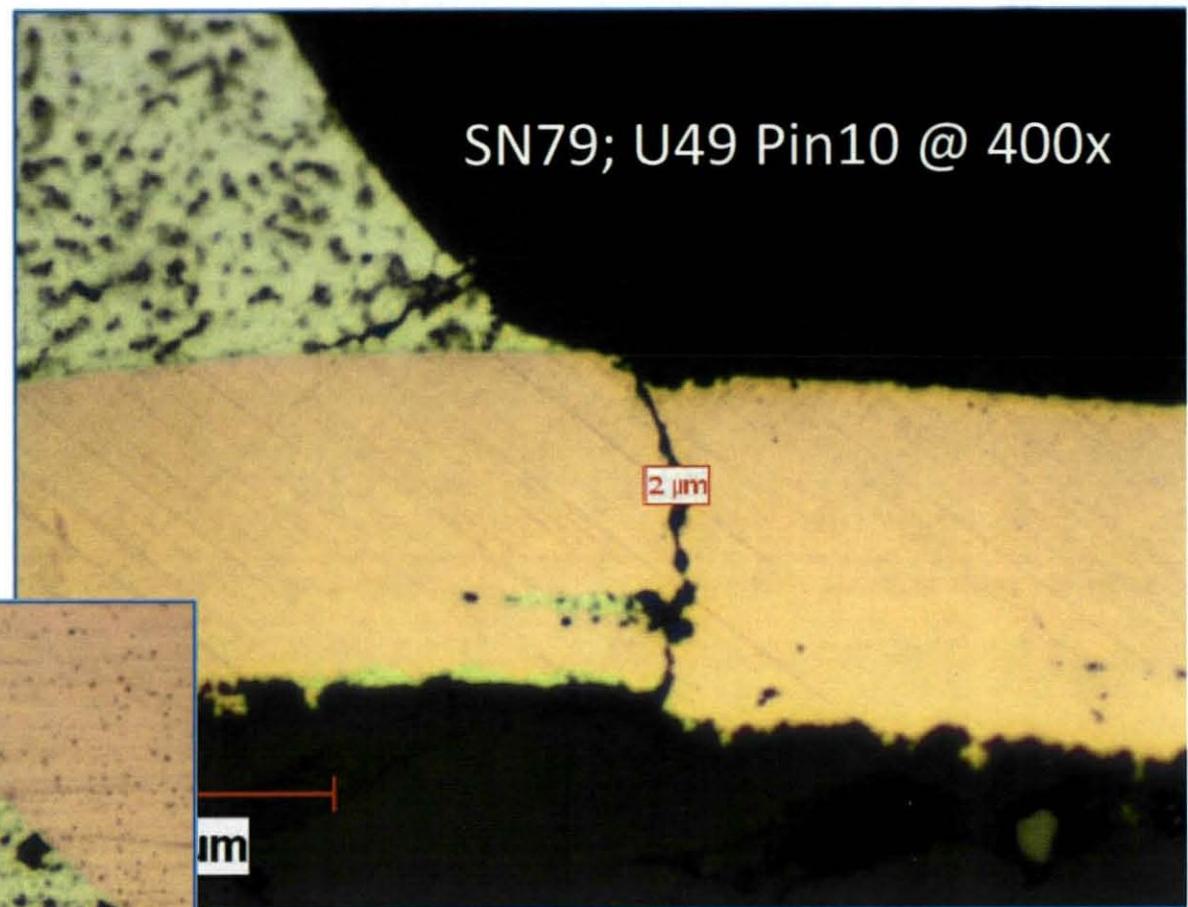
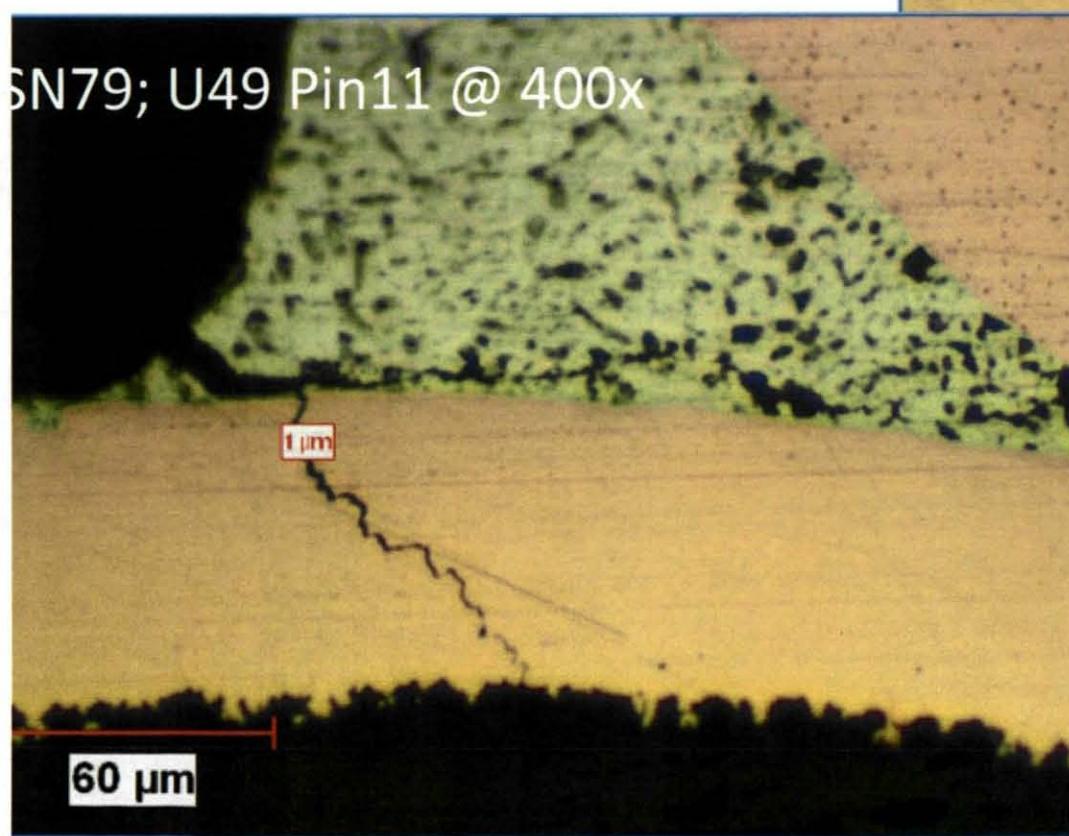


SN67, U31, left lead solder crack, 100x



SN 79, U49, pin 11, 100x

Vibration Testing



Testing Activities

NASA-DoD Test Vehicles

Specific testing details can be found in the Joint Test Protocol (JTP)

http://www.teerm.nasa.gov/projects/NASA_DODLeadFreeElectronics_Proj2.html

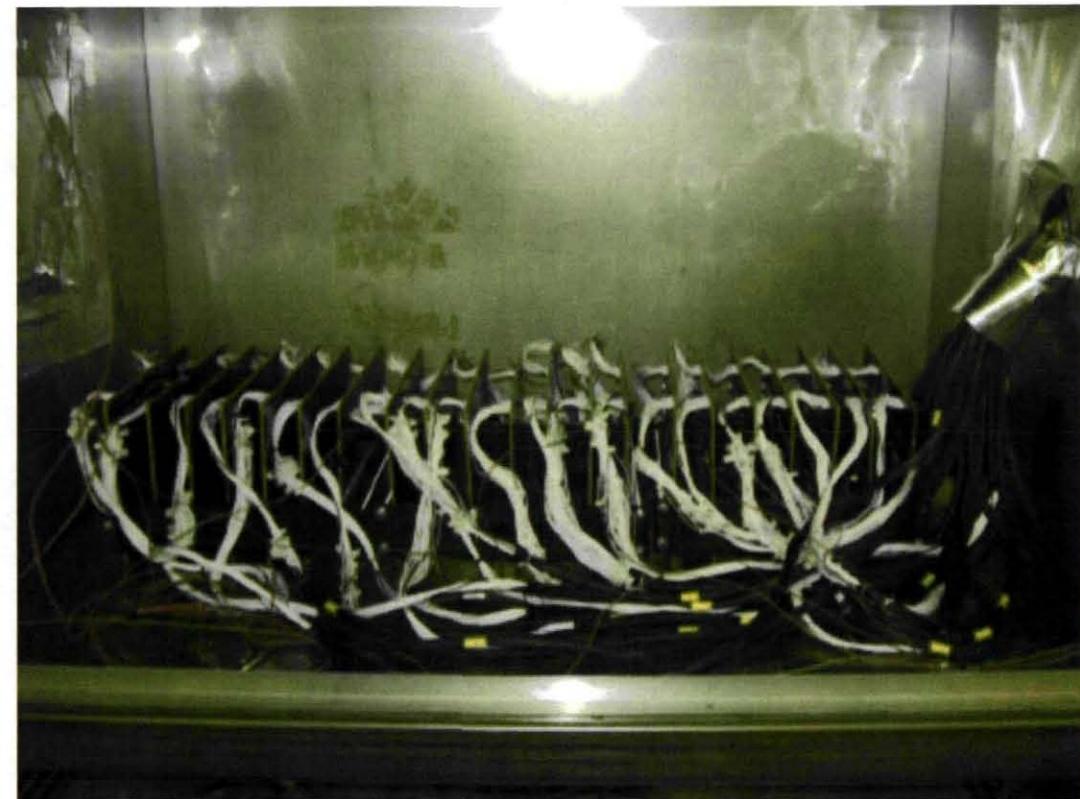
- Thermal Cycle Testing (-20/+80°C)  **BOEING** COMPLETE
- Combine Environments Testing **Raytheon** COMPLETE
- Drop Testing  **CELESTICA**. COMPLETE
- Thermal Cycle Testing (-55/+125°C)  **Rockwell Collins** COMPLETE
- Vibration Testing  **BOEING** COMPLETE
- Mechanical Shock Testing  **BOEING** COMPLETE
- Interconnect Stress Test (IST)  COMPLETE
- Copper Dissolution  **CELESTICA**.  COMPLETE

Thermal Cycle Testing (-20/+80°C)



Test Parameters

- 5 to 10°C/minute ramp
- 30 minute dwell at 80°C
- 10 minute dwell at -20°C



~ 7,000 Thermal Cycles
Completed

Thermal Cycle Testing (-55/+125°C)

**Rockwell
Collins**

Test Parameters

- 5 to 10°C/minute ramp
- 30 minute dwell at 125°C
- 10 minute dwell at -55°C



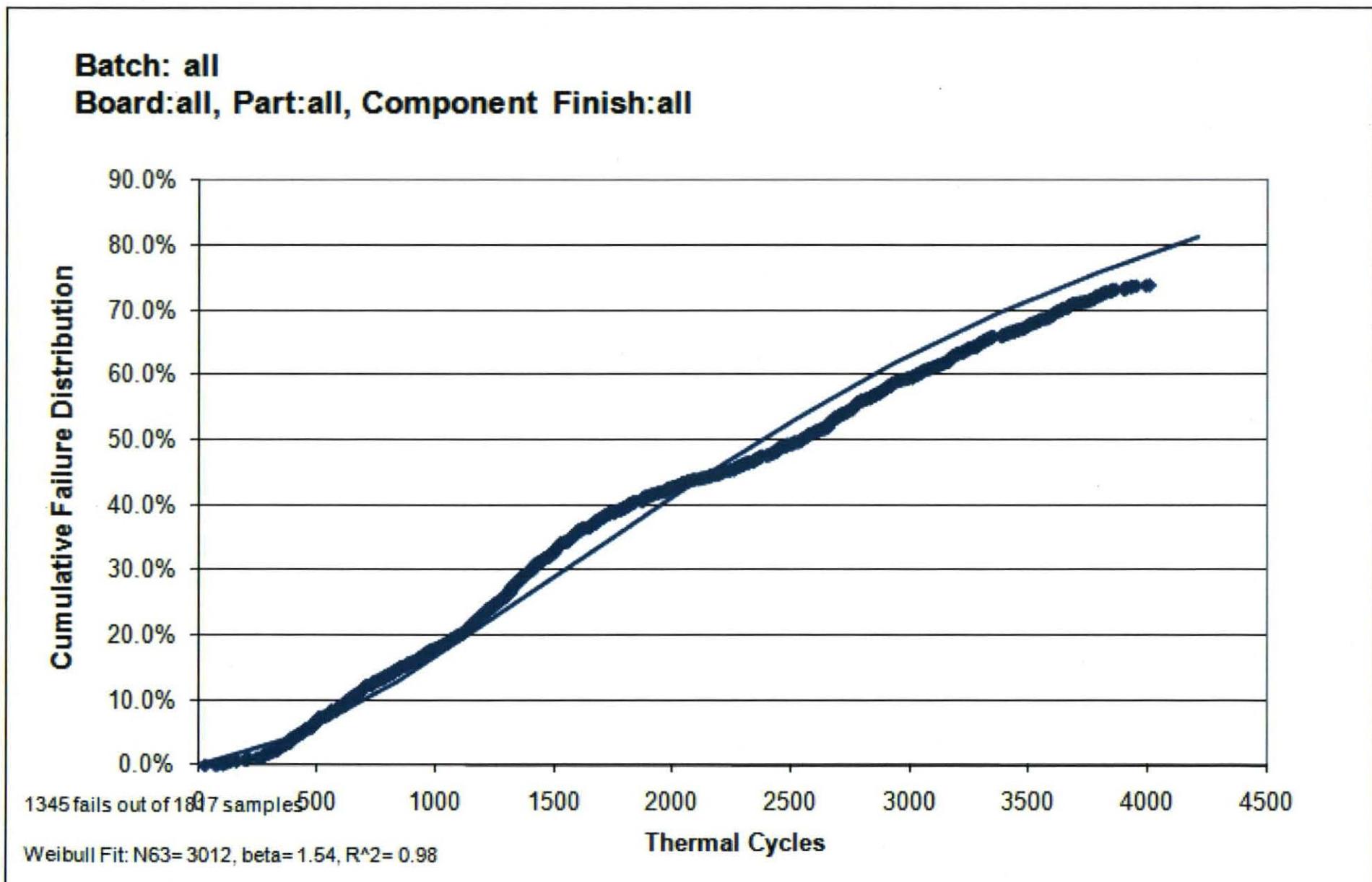
**~4,000 Thermal Cycles
Completed**

Thermal Cycle Testing (-55/+125°C)

**Rockwell
Collins**

Data Snapshot from “Manufactured” Test Vehicles

- No “Rework” Data



Thermal Cycle Testing (-55/+125°C)

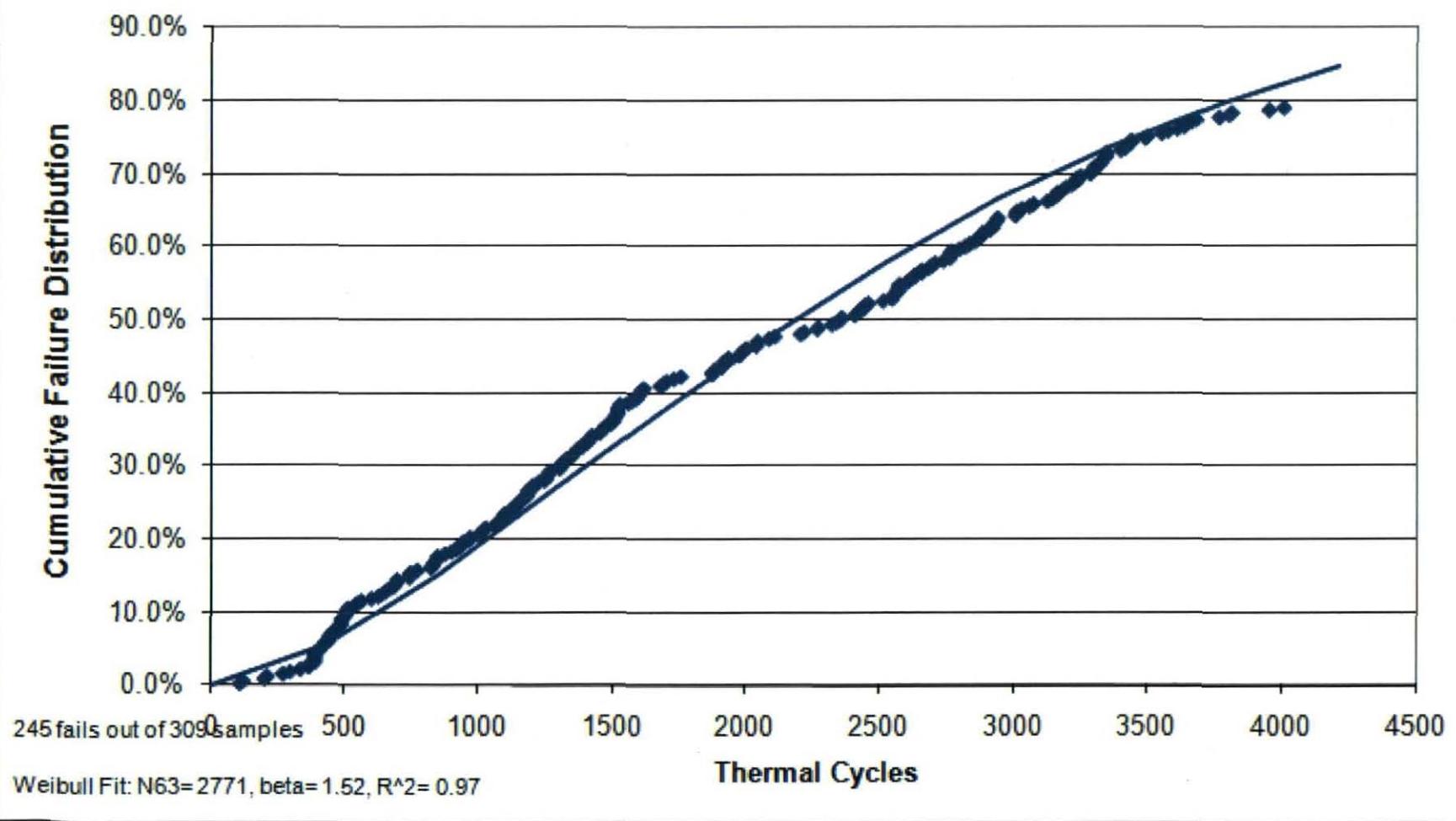
**Rockwell
Collins**

Data Snapshot from “Manufactured” Test Vehicles

- No “Rework” Data
- TQFP-144

Batch: all

Board:all, Part:TQFP-144, Component Finish:all



Thermal Cycle Testing (-55/+125°C)

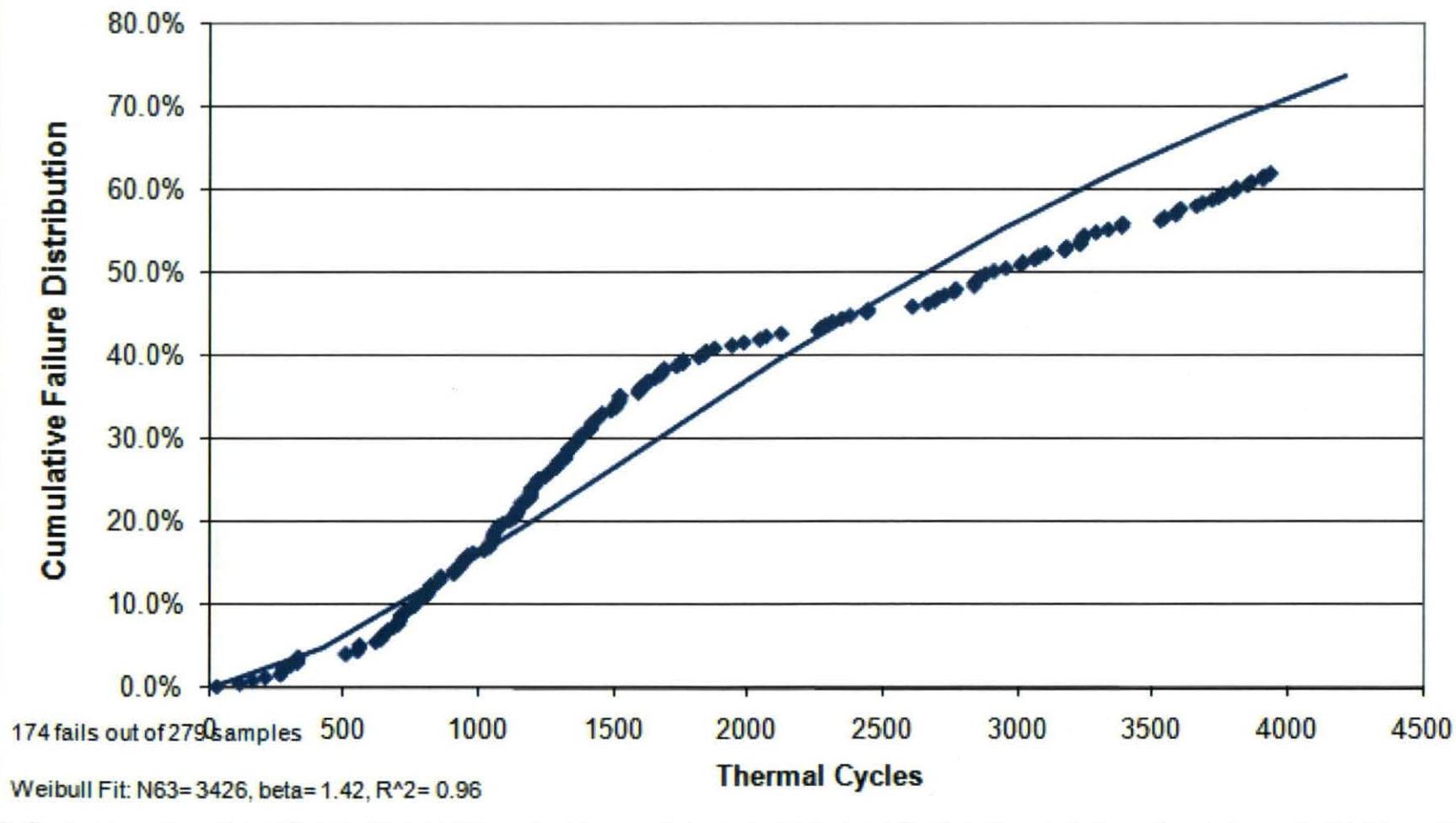
Rockwell
Collins

Data Snapshot from “Manufactured” Test Vehicles

- No “Rework” Data
- BGA-225

Batch: all

Board:all, Part:BGA-225, Component Finish:all



Thermal Cycle Testing (-55/+125°C)

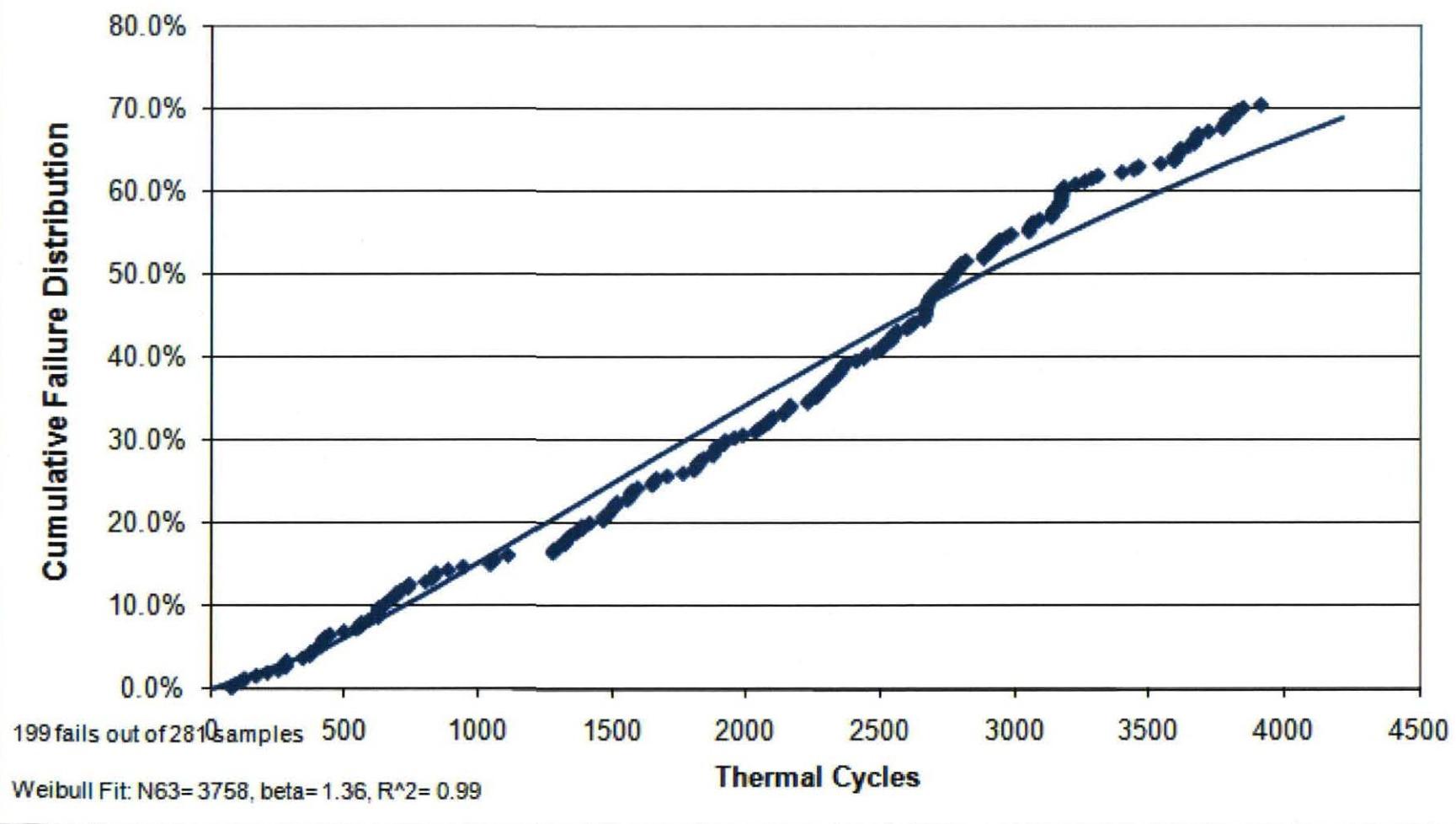
**Rockwell
Collins**

Data Snapshot from “Manufactured” Test Vehicles

- No “Rework” Data
- CSP-100

Batch: all

Board:all, Part:CSP-100, Component Finish:all



Thermal Cycle Testing (-55/+125°C)

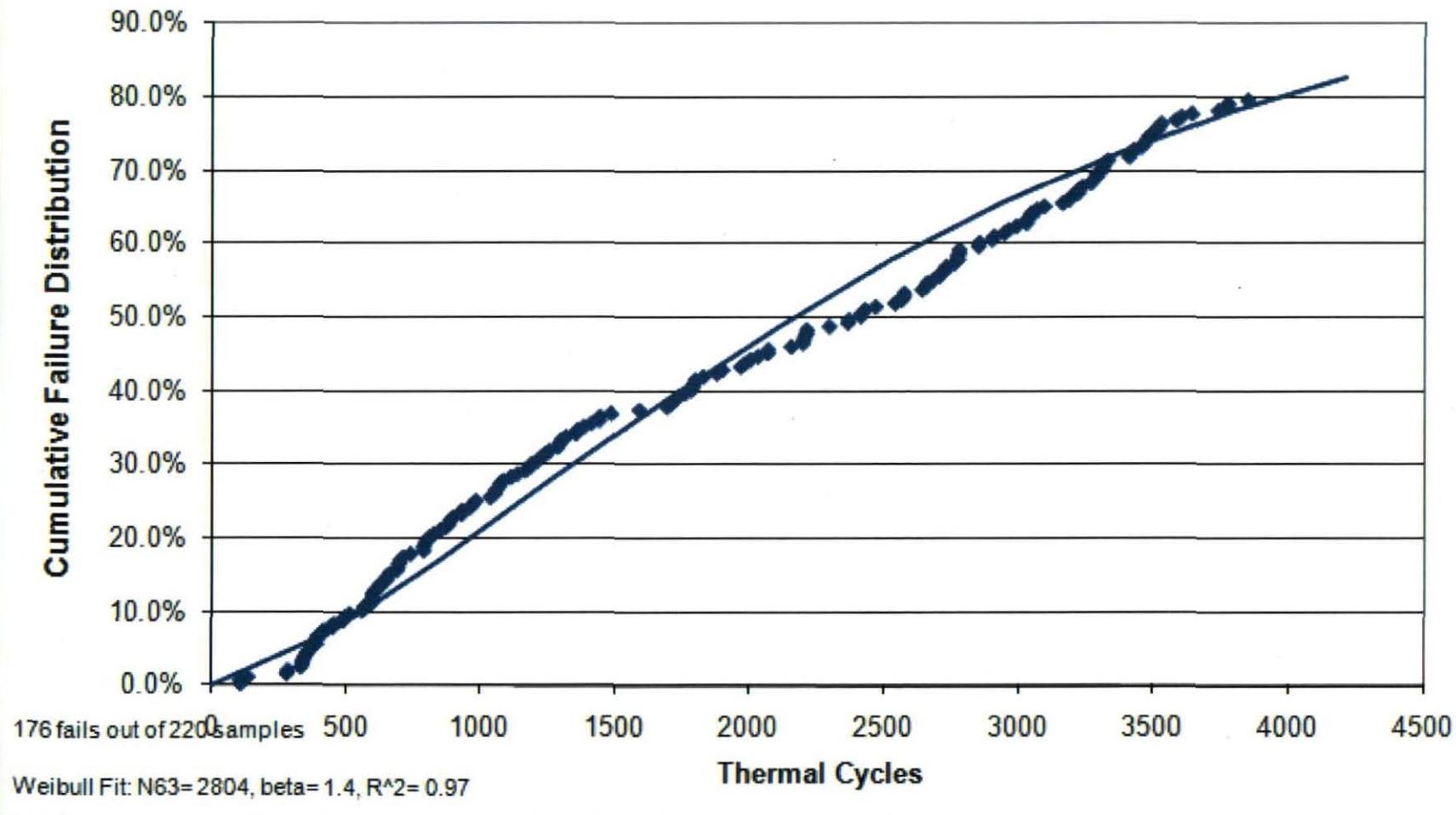
**Rockwell
Collins**

Data Snapshot from “Manufactured” Test Vehicles

- No “Rework” Data
- PDIP-20

Batch: all

Board:all, Part:PDIP-20, Component Finish:all



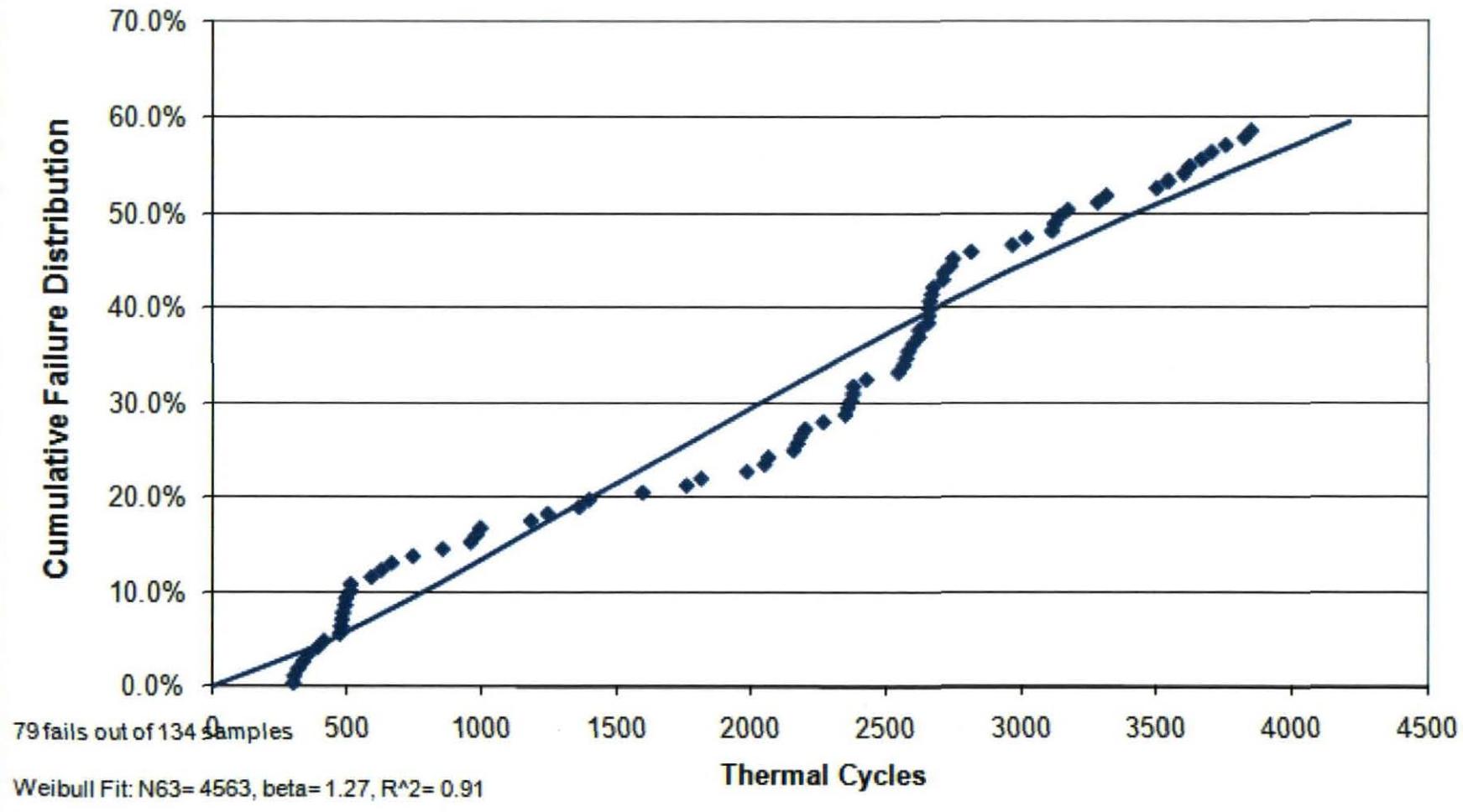
Thermal Cycle Testing (-55/+125°C)

**Rockwell
Collins**

Data Snapshot from “Manufactured” Test Vehicles

- No “Rework” Data
- QFN

Batch: all
Board:all, Part:QFN, Component Finish:all



Combine Environments Testing

Raytheon

Thermal Cycle with Vibration

- -55°C to +125°C
- 20°C/minute ramp
- 15 minute dwell at -55°C and +125°C
- Vibration for the duration of the thermal cycle
- 10 g_{rms} pseudo-random vibration initially
- Increase vibration level 5 g_{rms} after every 50 cycles
- 55 g_{rms} maximum

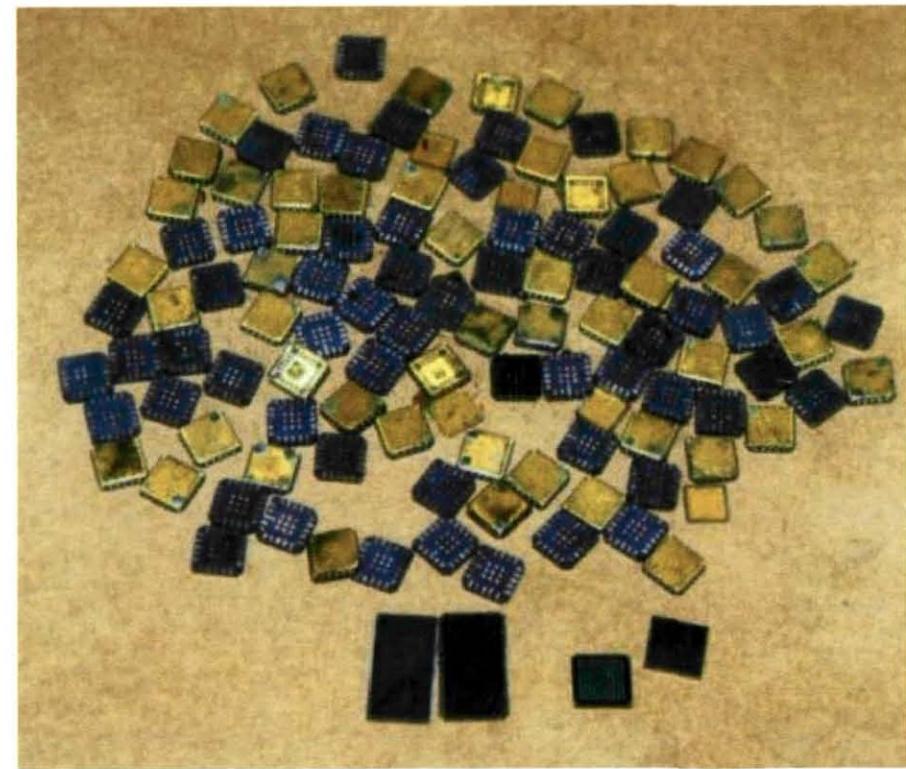
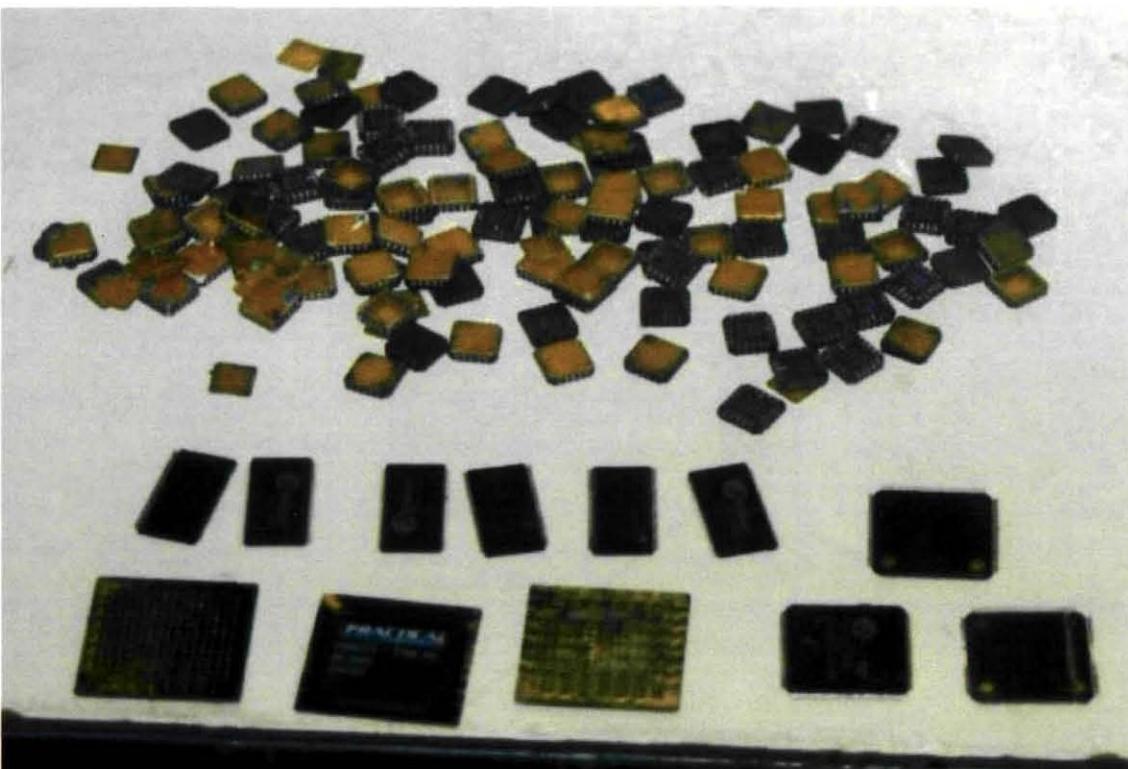


Combine Environments Testing

Raytheon

Overall, the component type had the greatest effect on solder joint reliability performance.

- The plated-through-hole components proved to be more reliable than the surface mount technology components.
- The plated-through-holes (PTH), PDIP-20, TQFP-144 and QFN-20 components performed the best.
- The BGA-225 components performed the worst.



Combine Environments Testing

Raytheon

Solder alloy had a secondary effect on solder joint reliability.

- In general, tin-lead finished components soldered with tin-lead solder paste were the most reliable with the exception of some components with lead contamination in the solder joints.
- In general, tin-silver-copper soldered components were less reliable than the tin-lead solder controls.
- In several cases, tin-silver-copper solder performed statistically as good as or equal to the baseline, eutectic tin-lead solder.

In general, reworked components were less reliable than the unreworked components. This is especially true with reworked lead-free CSP-100, reworked lead-free BGA-225

Combine Environments Testing



From this testing, it appears the selection of **component type and lead-free solder combinations** should be considered critical factors when considering converting to lead-free solder assembly, especially for surface mount technology design configurations.

Manufactured Test Vehicles

| Board Finish | Component | Finish | Solder | Number of Failed Components |
|--------------|-----------|----------|--------|-----------------------------|
| Im. Ag | BGA-225 | SAC405 | SAC305 | 76% (19 of 25) |
| | | | SN100C | 76% (19 of 25) |
| | | | SnPb | 92% (23 of 25) |
| | | SnPb | SAC305 | 84% (21 of 25) |
| | | | SN100C | 88% (22 of 25) |
| | | | SnPb | 60% (15 of 25) |
| | CLCC-20 | SAC305 | SAC305 | 96% (24 of 25) |
| | | | SN100C | 96% (24 of 25) |
| | | | SnPb | 92% (23 of 25) |
| | | SnPb | SAC305 | 100% (25 of 25) |
| | | | SN100C | 88% (22 of 25) |
| | | | SnPb | 84% (21 of 25) |
| Im. Ag | QFN-20 | Matte Sn | SAC305 | 20% (5 of 25) |
| | | | SN100C | 40% (10 of 25) |
| | | | SnPb | 20% (5 of 25) |
| Im. Ag | TQFP-144 | Matte Sn | SAC305 | 24% (6 of 25) |
| | | | SN100C | 52% (13 of 25) |
| | | | SnPb | 32% (8 of 25) |
| | | SnPb Dip | SAC305 | 0% (0 of 25) |
| | | | SN100C | 60% (15 of 25) |
| | | | SnPb | 8% (2 of 25) |

Combine Environments Testing



Rework Test Vehicles

| Board Finish | Component | Finish | Solder | New Component Finish | Rework Solder | Number of Failed Components |
|--------------|-----------|--------|--------|----------------------|---------------|-----------------------------|
| Im. Ag | BGA-225 | SAC405 | SAC305 | SAC405 | Flux Only | 60% (9 of 15) |
| | | | | | SnPb | 33% (5 of 15) |
| | | | SnPb | | | 50% (10 of 20) |
| | | SnPb | SAC305 | | | 65% (13 of 20) |
| | | | SnPb | SAC405 | SnPb | 80% (12 of 15) |
| | | | | SnPb | Flux Only | 20% (3 of 15) |
| | PDIP-20 | NiPdAu | SnPb | | | 7% (1 of 15) |
| | | Sn | SN100C | Sn | SN100C | 20% (2 of 10) |
| | | | | | | 7% (2 of 30) |
| | | SnPb | | | | 13% (2 of 15) |
| | | SnPb | SnPb | Sn | SnPb | 40% (4 of 10) |
| Im. Ag | TSOP-50 | Sn | SAC305 | Sn | SnPb | 60% (6 of 10) |
| | | | SnPb | | | 20% (3 of 15) |
| | | SnBi | SAC305 | SnBi | SAC305 | 90% (9 of 10) |
| | | | | | | 67% (10 of 15) |
| | | | SnPb | | | 33% (5 of 15) |
| | | SnPb | SAC305 | | | 33% (5 of 15) |
| | | | SnPb | Sn | SnPb | 50% (5 of 10) |
| | | | | SnPb | SnPb | 60% (6 of 10) |

Combine Environments Testing



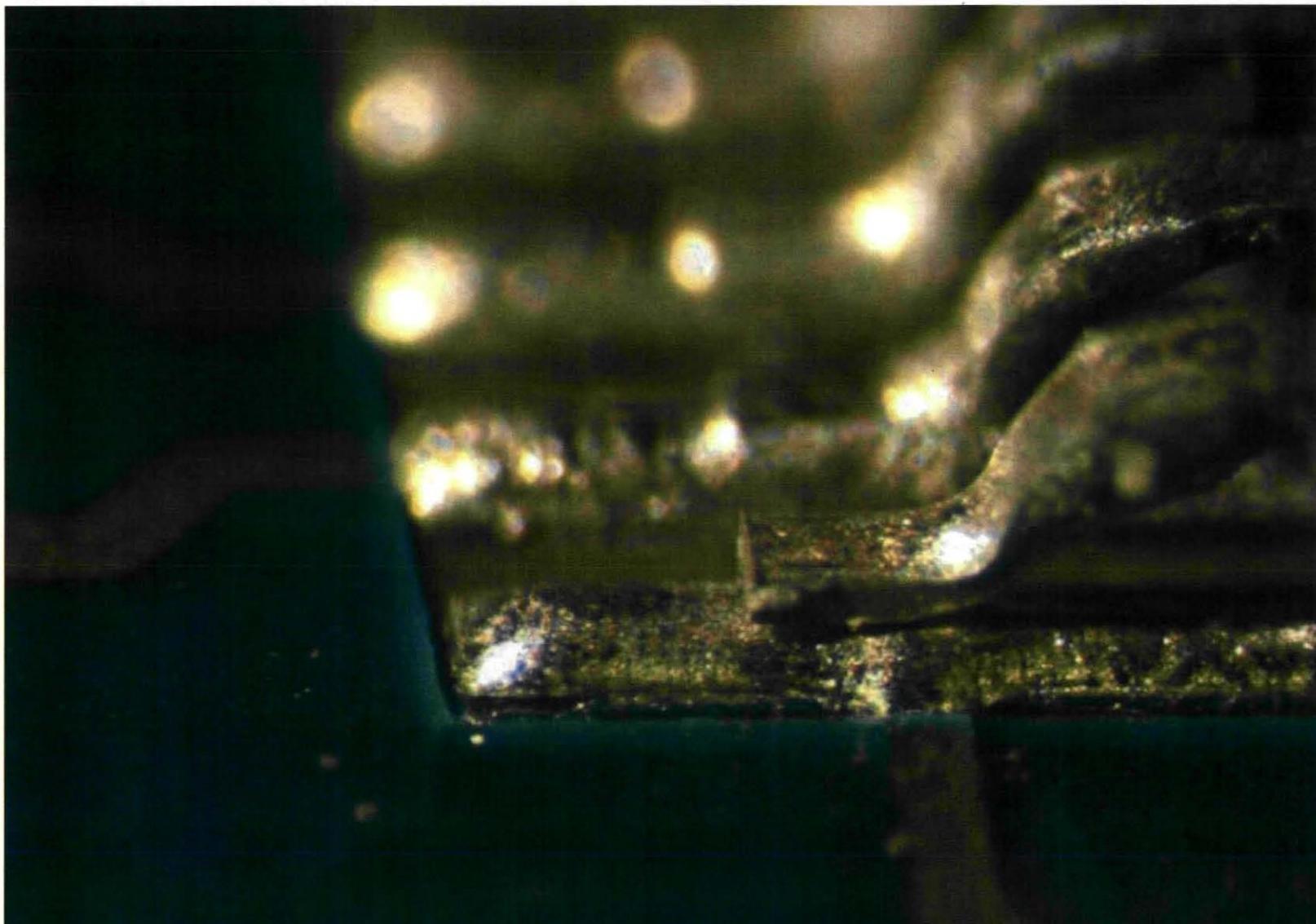
Failure Analysis In-Progress

| Failure Analysis Location | Test Vehicle | Component Location | Selection Criteria |
|---------------------------|--------------|--------------------|--|
| COM DEV | 21 | U34 | Mfg group - No signal, failed at 0 cycles |
| | 21 | U57 | Mfg group - Failed at cycle 1 |
| | 119 | U36 | Mfg group - Surrounded by components that fell off; failed at 233 cycles |
| | 119 | U39 | Mfg group - Surrounded by components that fell off; failed at 318 cycles |
| | 142 | U13 | Rwk group - Adjacent to rwked components, survived all 650 cycles |
| | 181 | U56 | Rwk group - Rwked component failed at cycle 1 |
| | 181 | U25 | Rwk group - Rwked component failed at cycle 1 |
| Lockheed Martin | 117 | U4 | Mfg group - Failed at 20 cycles; SN100C solder paste used |
| | 140 | U11 | Rwk group - Damaged pad from rwk - Failed at 398 cycles |
| | 183 | U41 | Rwk group - Failed at cycle 1, was not rwked |
| Nihon Superior | 23 | U30 | Mfg group - Survived 650 cycles, surrounded by components that fell off |
| | 23 | U43 | Mfg group - Failed at 120 cycles, located near center of TV |
| | 72 | U29 | Mfg group - Location in chamber (low fails); failed at 161 cycles |
| | 158 | U6 | Rwk group - Rwked component failed at cycle 1 |
| | 180 | U21 | Rwk group - Rwked component failed at cycle 1 |

Combined Environments Failure Analysis



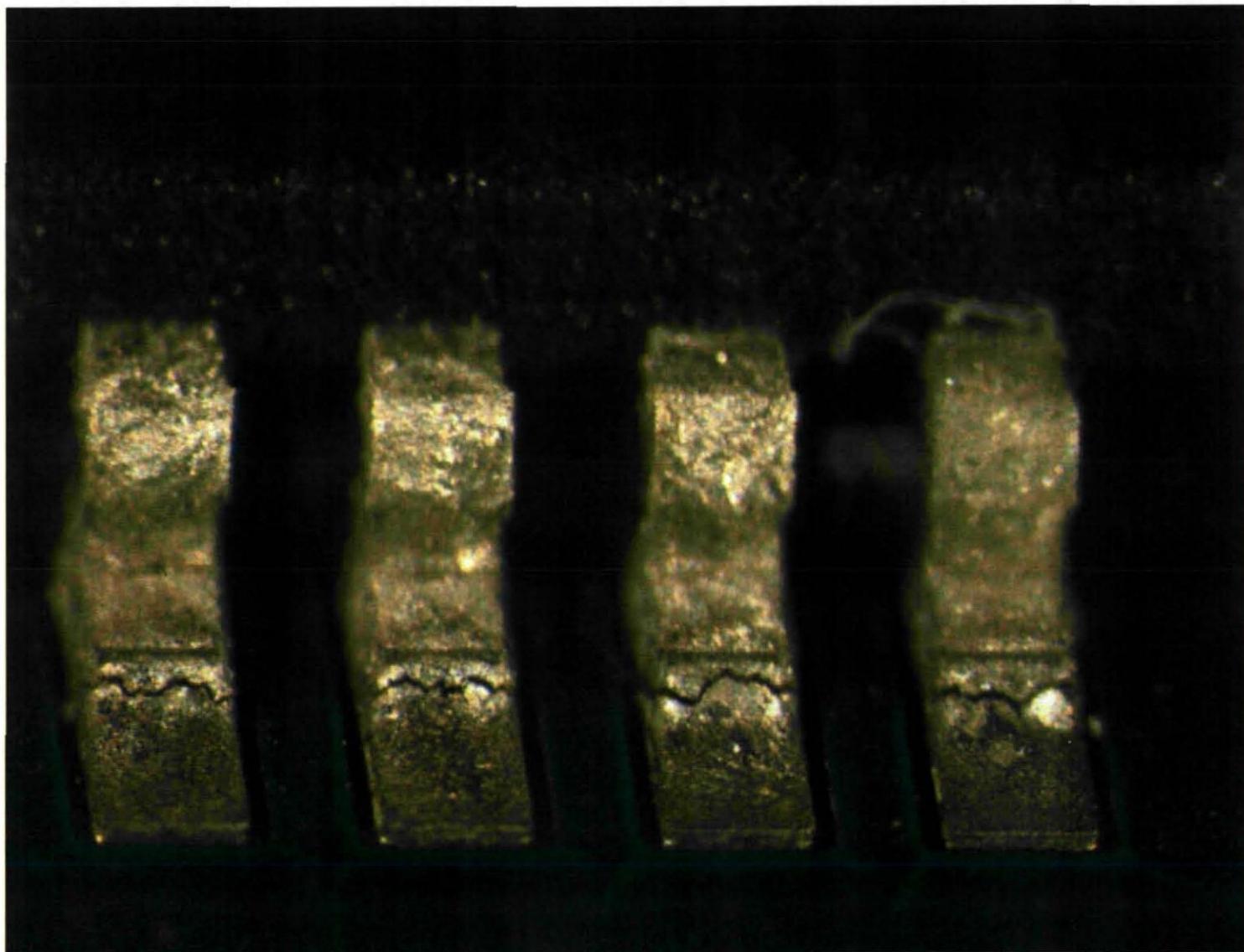
Test Vehicle 21; Component U34 – TQFP 144; Board Finish – Imm. Ag SnPb Manufactured (Batch C) - Solder (SnPb) - Component Finish (SnPb Dip): No signal, failed at 0 cycles



Combined Environments Failure Analysis



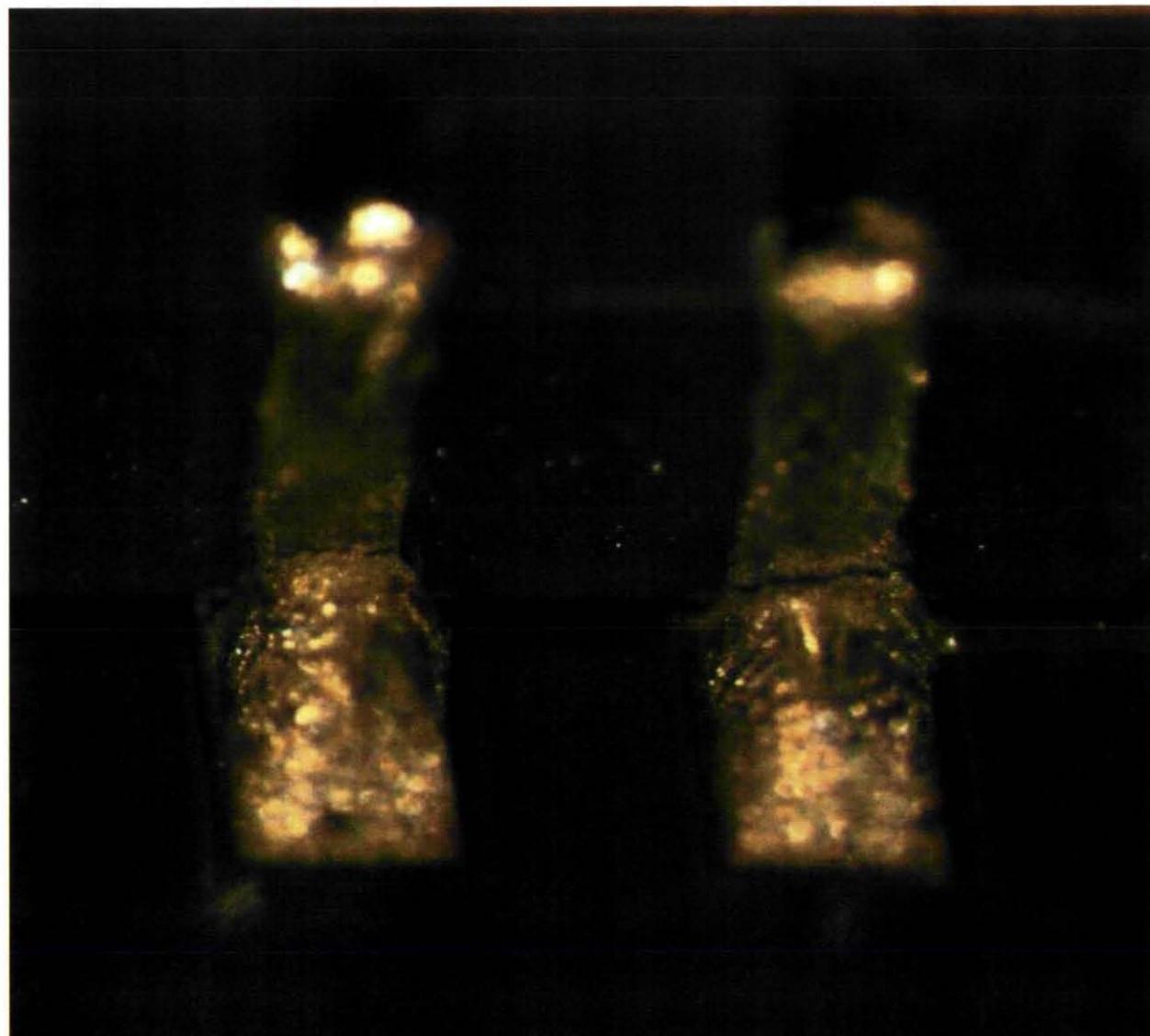
Test Vehicle 119; Component U39 – TSOP 50; Board Finish – Imm. Ag
Lead-Free Manufactured (Batch G) - Solder (SN100C) - Component Finish (SnPb)
Surrounded by components that fell off; failed at 318 cycles



Combined Environments Failure Analysis



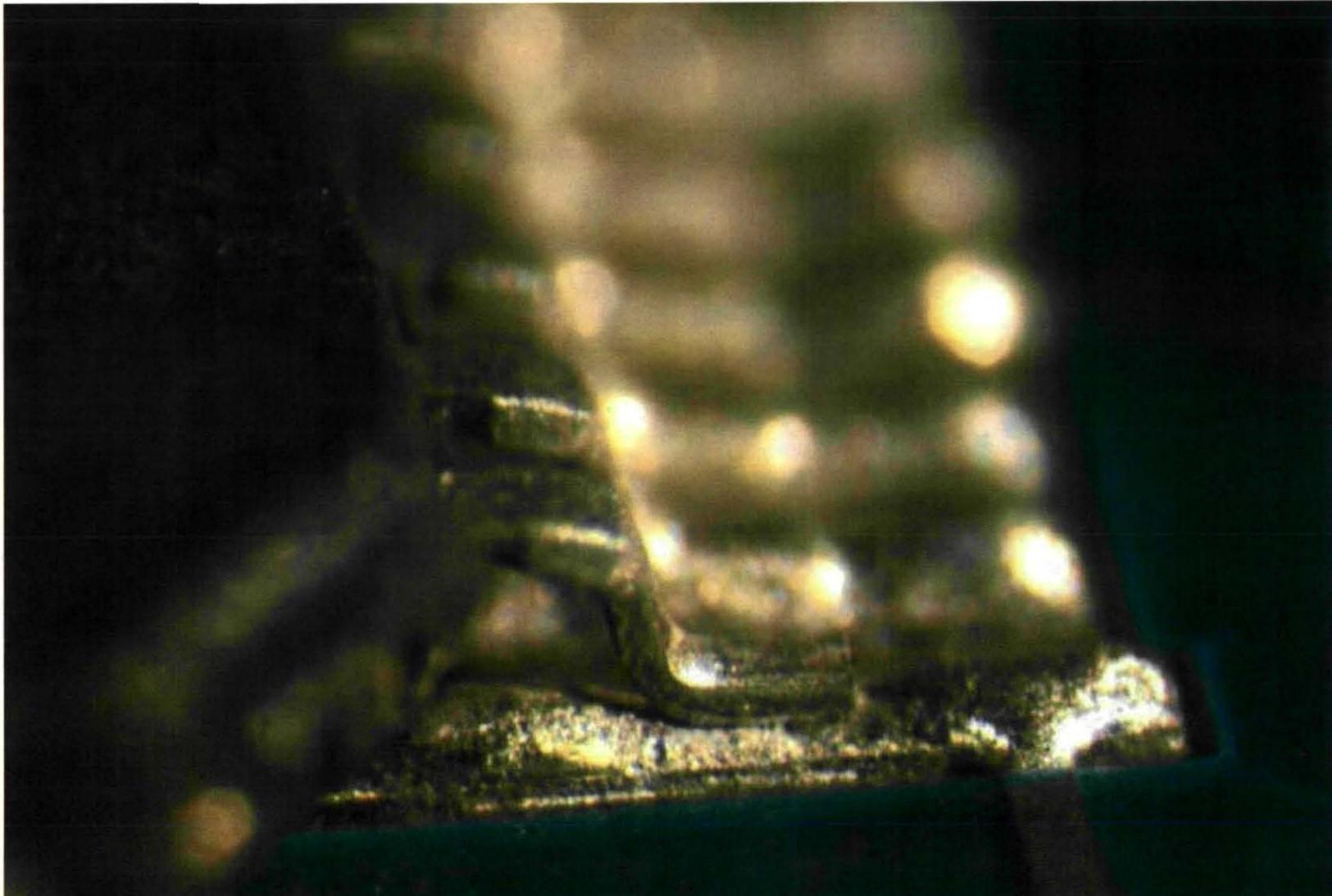
Test Vehicle 142; Component U13 – CLCC; Board Finish – Imm. Ag SnPb Rework (Batch B) - Solder (SnPb) - Component Finish (SAC305)
Adjacent to reworked components, survived all 650 cycles



Combined Environments Failure Analysis



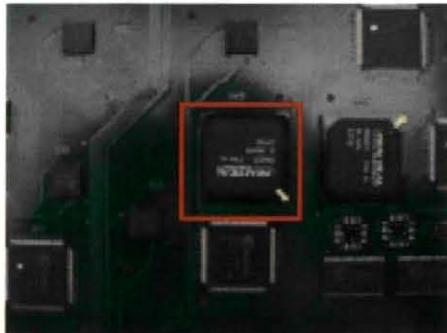
Test Vehicle 21; Component U57 – TQFP 144; Board Finish – Imm. Ag SnPb Manufactured (Batch C) - Solder (SnPb) - Component Finish (SnPb Dip)
Failed at cycle 1



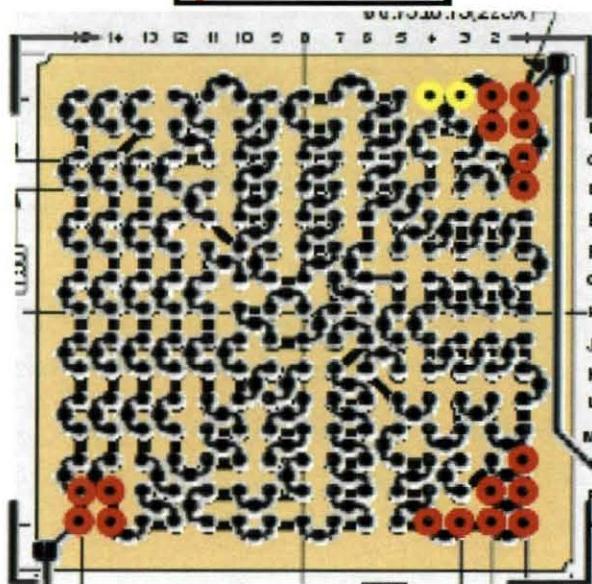
Combined Environments Failure Analysis

Test Vehicle 23

SnPb Manufactured
Ag-SnPb-SnPb

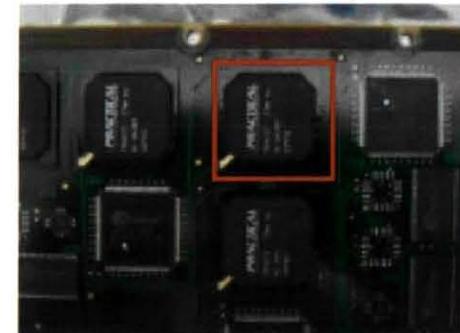


② U43(BGA225)

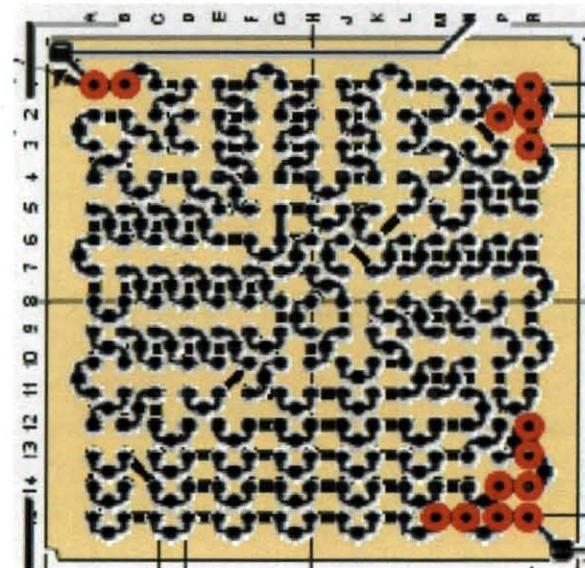


Test Vehicle 158

SnPb REWORK
ENIG-SnPb-SnPb

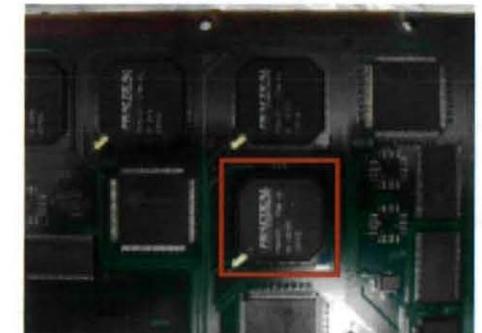


④ U6(BGA225)

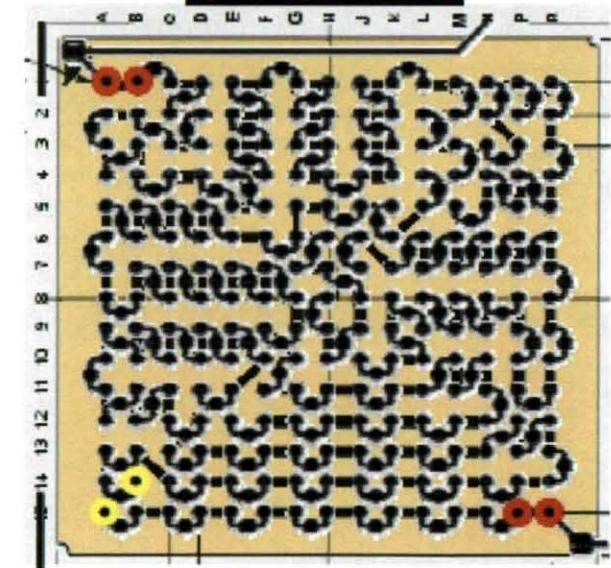


Test Vehicle 180

Pb-Free REWORK
Ag-SAC305-SnCu



⑤ U21(BGA225)

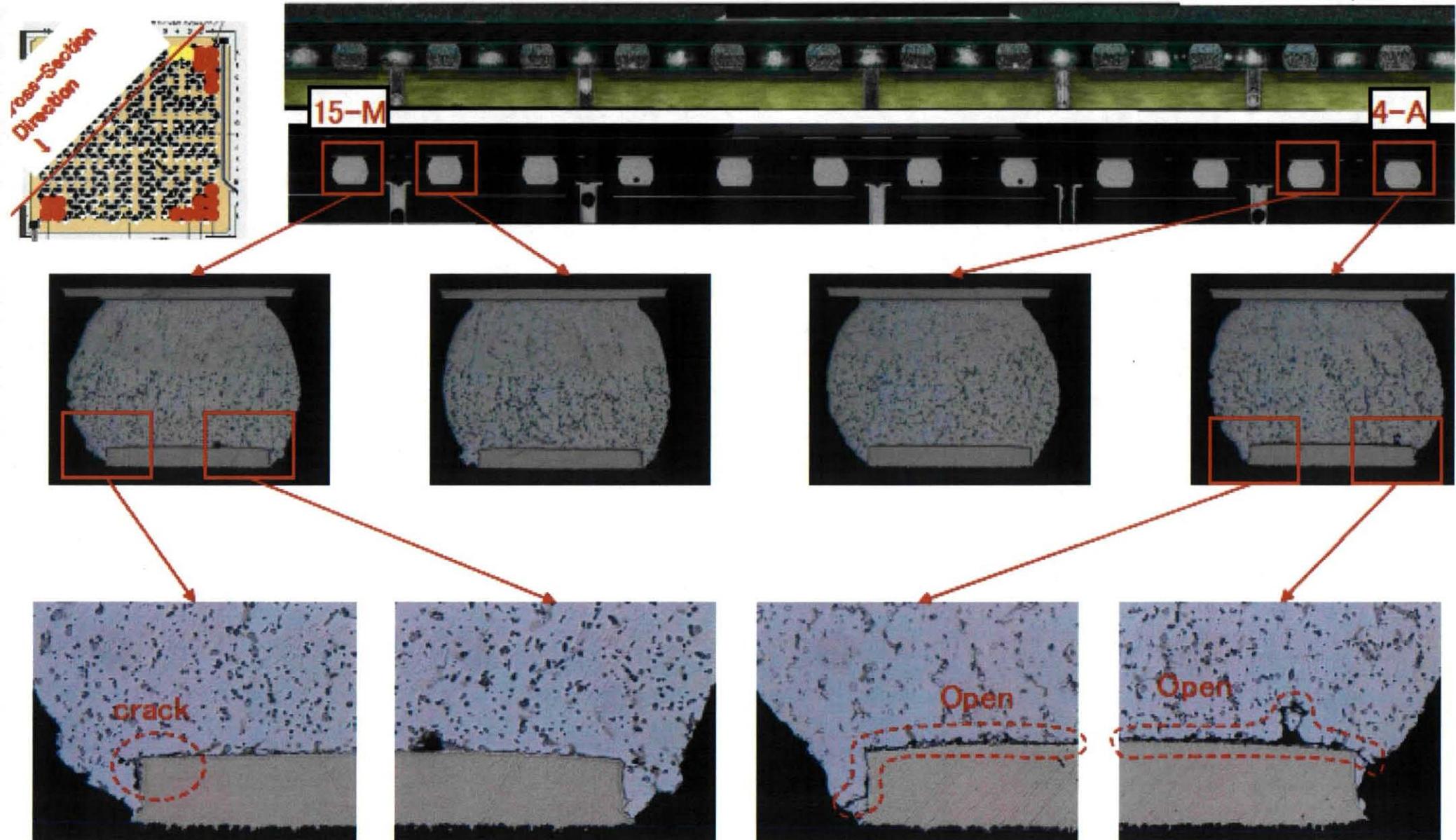


○ :Open

○ :High resistance

Combined Environments Failure Analysis

SAC405 solder balls / SnPb solder paste / SnPb reflow profile



Mechanical Shock Testing



Project representatives felt that only testing in the Z-axis was required as this is the only axis which allows significant board bending and subsequent solder joint failures.

| Parameters | The shock transients will be applied perpendicular to the plane of the board and will be increased after every 100 shocks (i.e., a step stress test). For Level 6 (300 G's), 400 shocks will be applied. Frequency range is 40 to 1000 Hz. SRS damping: 5% | | | |
|---|--|-----------------|----------------|------------------|
| | Test Shock Response Spectra | Amplitude (G's) | Te (msec) | Shocks per Level |
| | Modified Functional Test for Flight Equipment (Level 1) | 20 | <30 | 100 |
| | Modified Functional Test for Ground Equipment (Level 2) | 40 | <30 | 100 |
| | Modified Crash Hazard Test for Ground Equipment (Level 3) | 75 | <30 | 100 |
| | Level 4 | 100 | <30 | 100 |
| | Level 5 | 200 | <30 | 100 |
| | Level 6 | 300 | <30 | 400 |
| Number of Test Vehicles Required | | | | |
| Manufactured | | Rework | | |
| Mfg. SnPb | Mfg. LF | Rwk. SnPb | Rwk. SnPb ENIG | Rwk. LF |
| 5 | 5 | 5 | 1 | 5 |
| Trials per Specimen | | 1 | | |

Mechanical Shock Testing



Mechanical Shock Testing



- The very first components to fail were lead-free PDIP components
 - Lead cracking in the fillet area is being observed as well as some trace cracking near the corner leads. It is not possible to determine if one event happened before the other or if the events are happening simultaneously.
- All of the test vehicles passed the first 3 levels of testing which were conducted per MIL-STD-810F, Method 516.5; Modified Functional Test for Flight Equipment (Level 1), Modified Functional Test for Ground Equipment (Level 2), and Modified Crash Hazard Test for Ground Equipment (Level 3).
 - 100 shocks were conducted in the z-axis for each of the three levels, equating to conducting each of the three tests 33 times.
- It appears that the predominant failure mechanism for the BGA components was pad cratering no matter the solder alloy; lead-free or SnPb.

Mechanical Shock Testing



In general SAC305 performed as well as the SnPb for surface mount components.

| Component | % of Components Failed During Mechanical Shock Testing | | | |
|-----------|--|---------|------------------------|---------|
| | "Manufactured" Test Vehicles | | "Rework" Test Vehicles | |
| | SnPb | Pb-Free | SnPb | Pb-Free |
| BGA-225 | 94 | 96 | 95 | 100 |
| CLCC-20 | 22 | 30 | 22 | 30 |
| CSP-100 | 32 | 26 | 42 | 38 |
| PDIP-20 | 53 | 73 | 54 | 58 |
| QFN-20 | 0 | 10 | 0 | 0 |
| TQFP-144 | 70 | 62 | 68 | 80 |
| TSOP-50 | 4 | 0 | 22 | 20 |

Mechanical Shock Testing



| | Relative Ranking (Solder Alloy / Component Finish) | | | | | | | | |
|----------|--|-------------------|-------------------|-------------------|--------------------------|--------------------------|-------------------------------------|--|--|
| | Sn37Pb/ Sn37Pb | SAC305/ SAC405 | Sn37Pb/ SAC405 | SAC305/ Sn37Pb | Rwk Flux Only/ Sn37Pb | Rwk Flux Only/ SAC405 | Rwk Sn37Pb/SAC405 (SnPb Profile) | Rwk Sn37Pb/SAC405 (Pb-Free Profile) | |
| BGA-225 | 1 | 1 | 2 | 1 | 1 | 1 | 2 | 1 | |
| CLCC-20 | Sn37Pb/ Sn37Pb | SAC305/ SAC305 | Sn37Pb/ SAC305 | SAC305/ Sn37Pb | | | | | |
| CSP-100 | 1 | 2 | 2 | 2 | | | | | |
| PDIP-20 | Sn37Pb/ SnPb | SN100C/ Sn | Sn37Pb/ NiPdAu | Rwk Sn37Pb/ Sn | Rwk Sn100C/ Sn | | | | |
| QFN-20 | 1 | 1 | 1 | 2 | 2 | | | | |
| TQFP-144 | Sn37Pb/ Sn | SAC305/ Sn | Sn37Pb/ NiPdAu | SAC305/ NiPdAu | Sn37Pb/ Sn37Pb Dip | SAC305/ SAC305 Dip | | | |
| TSOP-50 | 1 | 1 | 1 | 1 | 1 | 2 | | | |
| | X | X | X | X | | | | | |

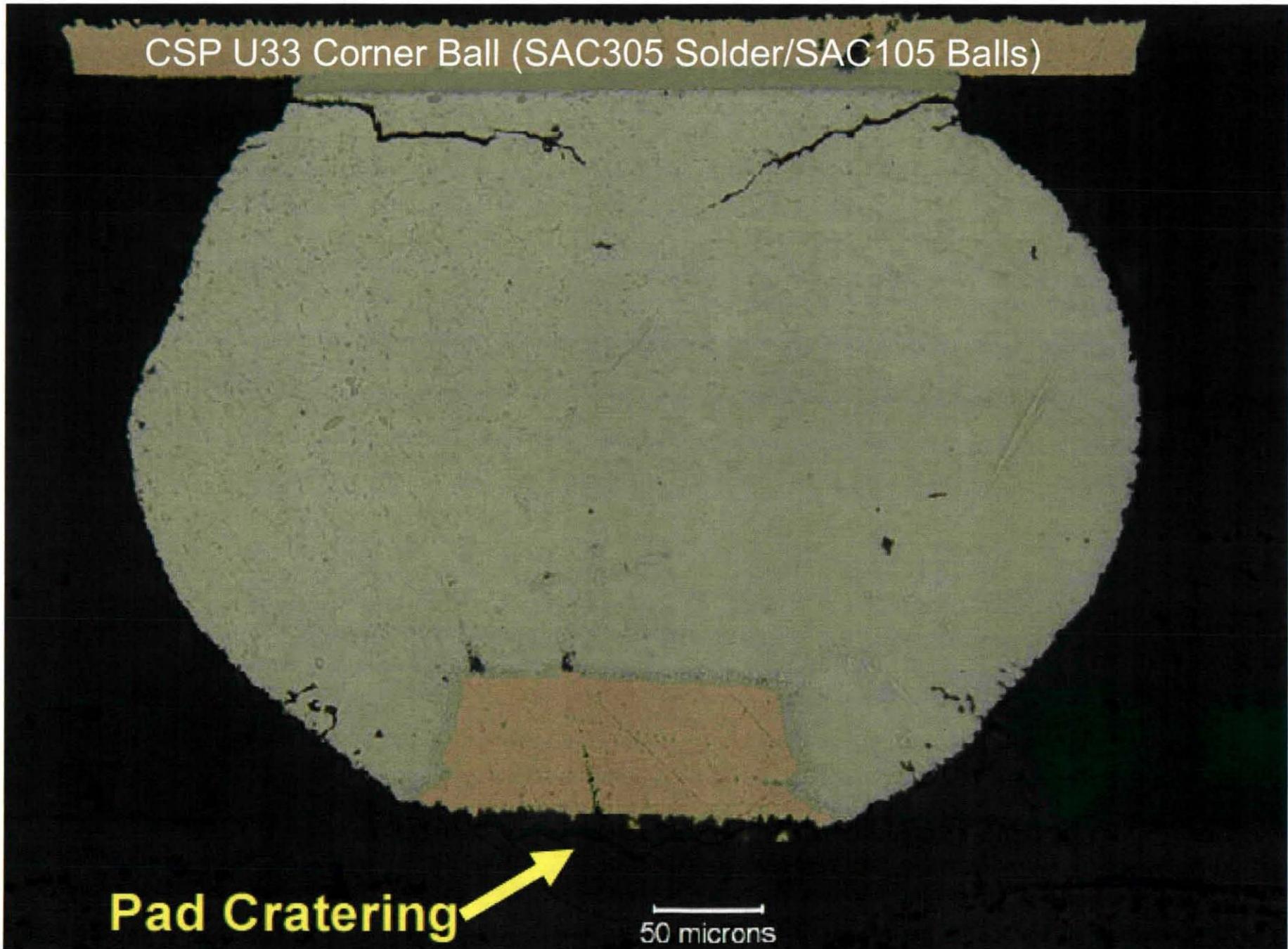
X = Not enough failures to rank

1 = as good as or better than Sn37Pb control

2 = worse than Sn37Pb control

3 = much worse than Sn37Pb control

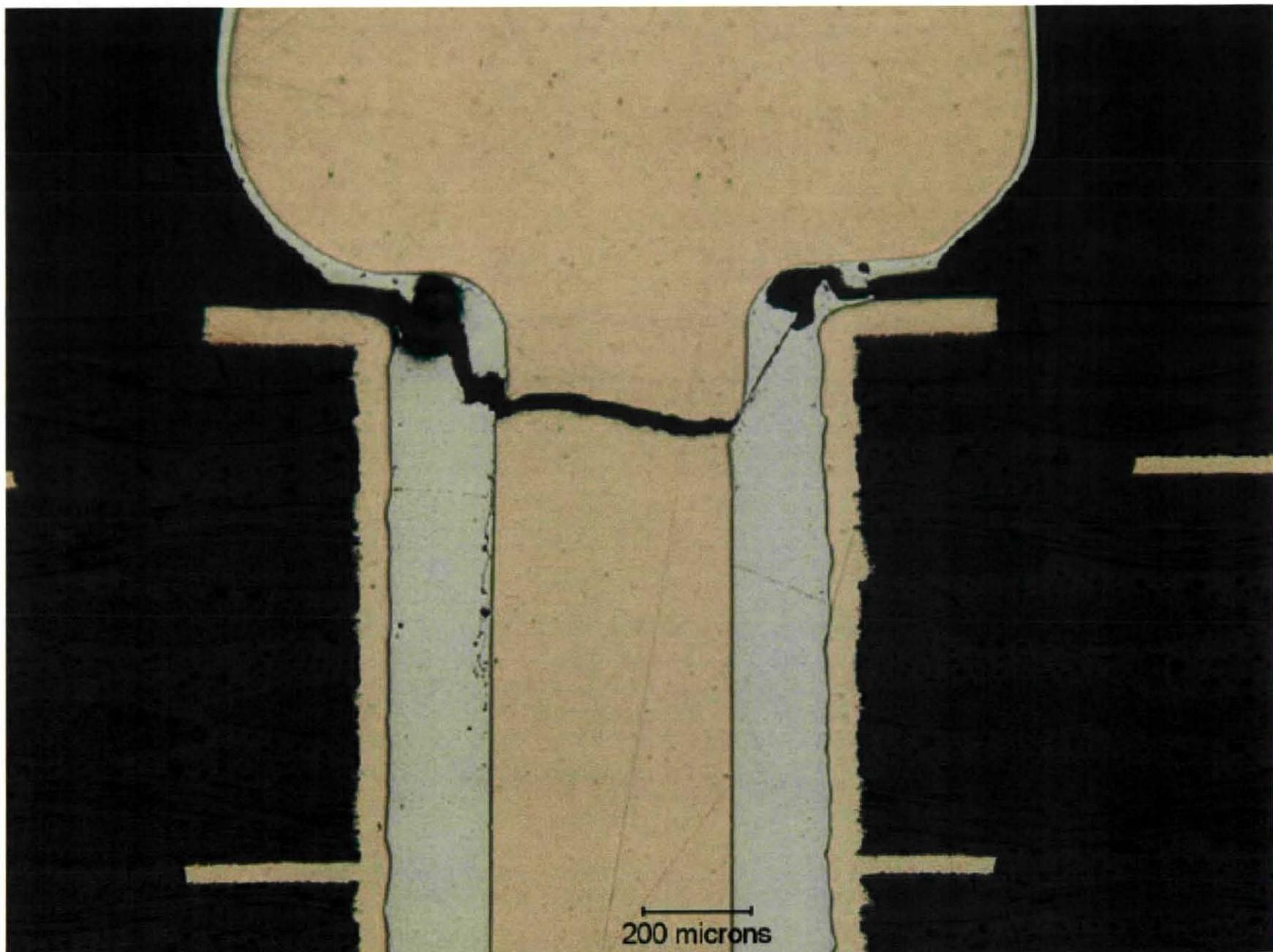
Mechanical Shock Testing



Mechanical Shock Testing



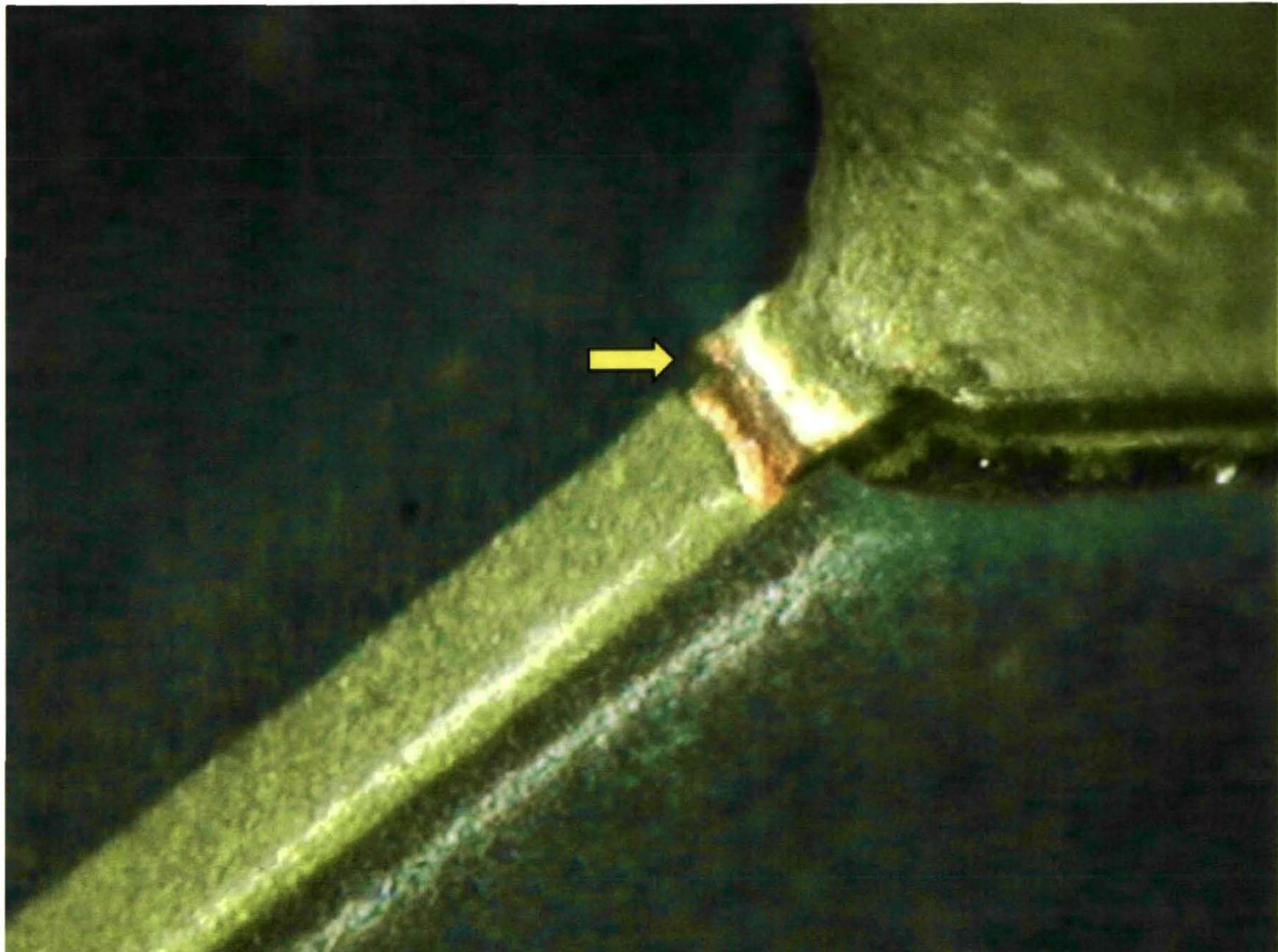
PDIP U8 Corner Lead (SN100C Solder/Sn Finish)



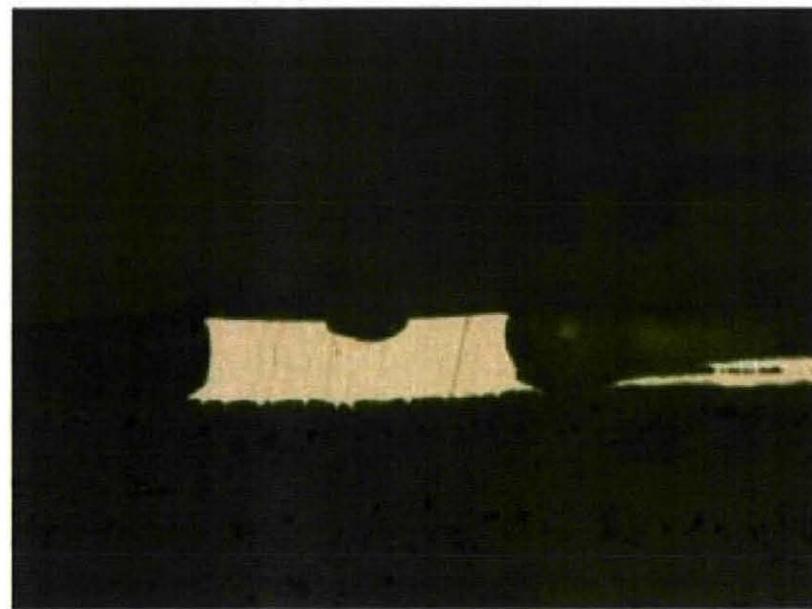
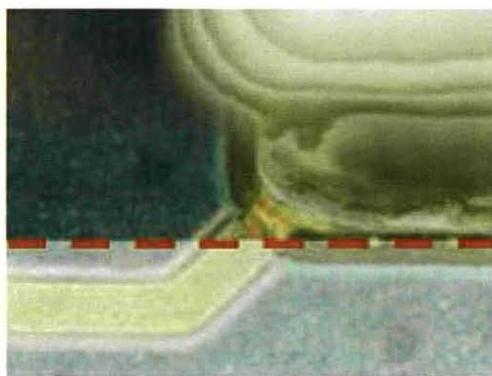
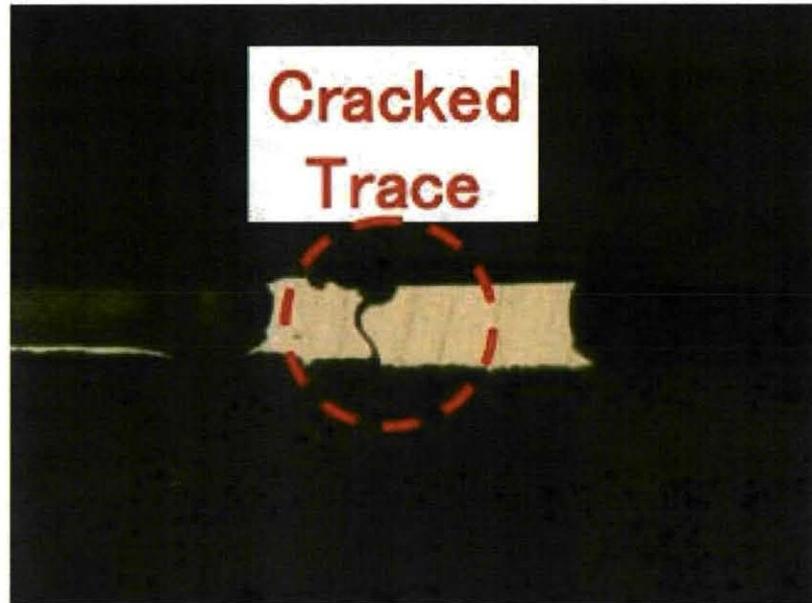
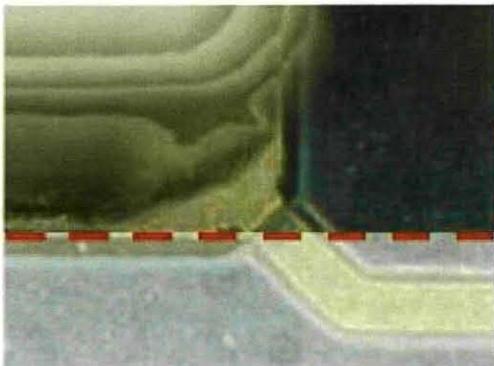
Mechanical Shock Testing



PDIP U38 Trace Crack (SN100C)



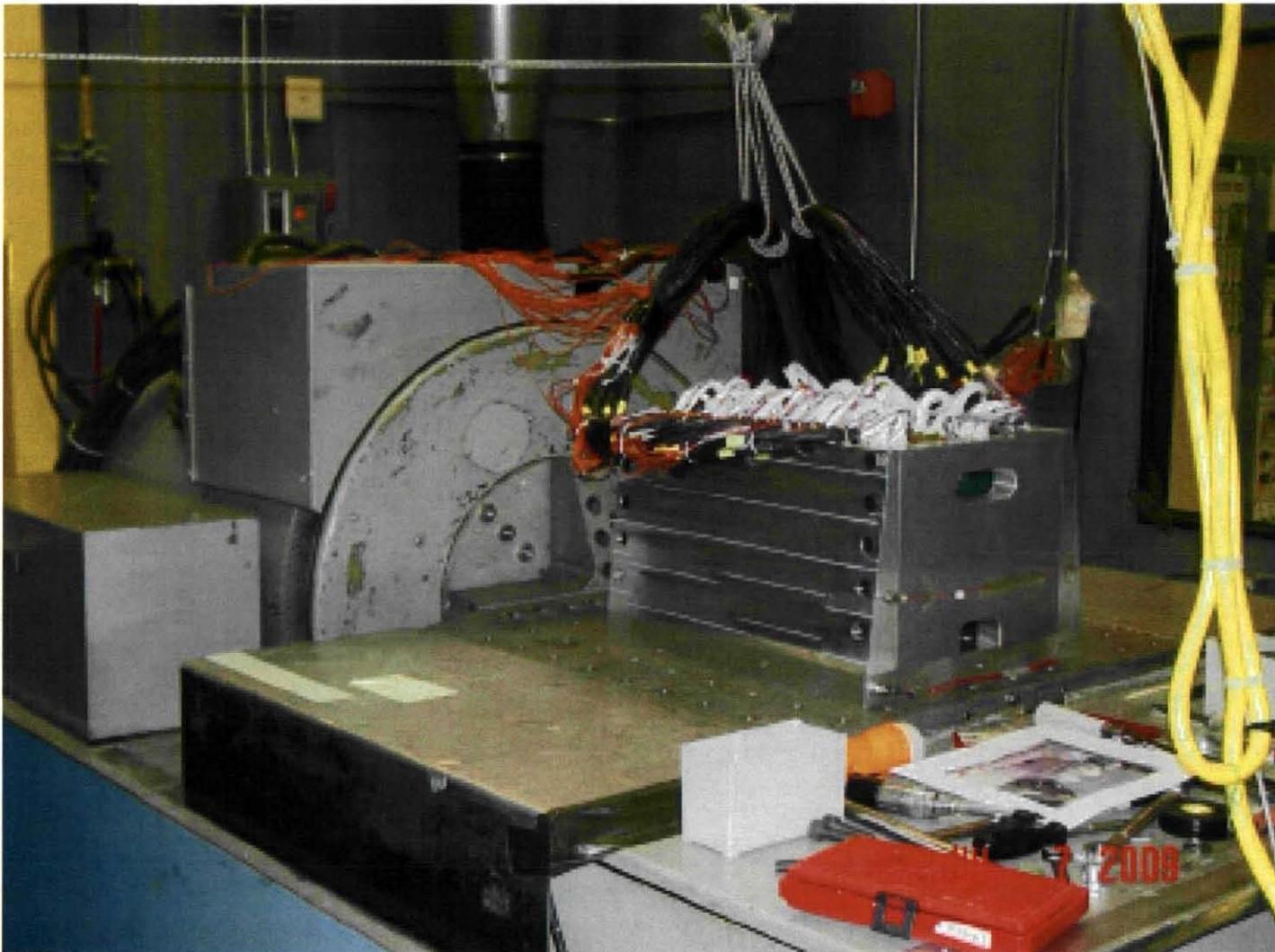
Mechanical Shock Testing



Vibration Testing



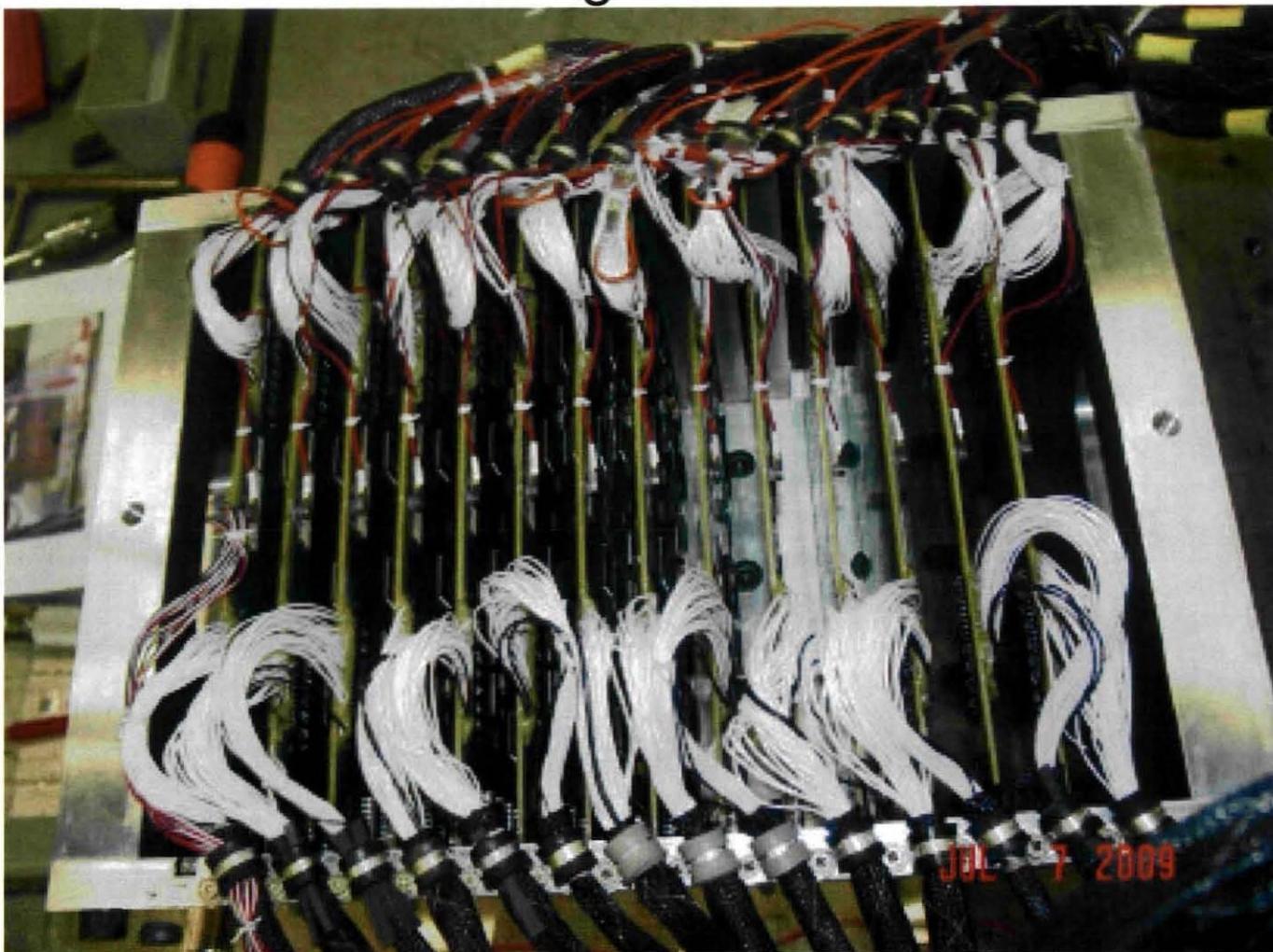
Subject the test vehicles to 8.0 g_{rms} for one hour. Then increase the Z-axis vibration level in 2.0 g_{rms} increments, shaking for one hour per step until the 20.0 g_{rms} level is completed. Then subject the test vehicles to a final one hour of vibration at 28.0 g_{rms}.



Vibration Testing



- Very early PDIP failures were observed.
- At an initial glance, the data does not look much different than the JCAA/JGPP test results.
- There **does** seem to be a big difference between solder alloys.



Vibration Testing



% of Components Failed During Vibration Testing

(Includes Mixed
Solders)

| Component | "Manufactured" Test Vehicles | | | "Rework" Test Vehicles | |
|-----------|------------------------------|--------------|--------------|------------------------|---------------|
| | SnPb Paste | SAC305 Paste | SN100C Paste | SnPb Paste | Pb-Free Paste |
| BGA-225 | 84 | 98 | 100 | 100 | 100 |
| CLCC-20 | 32 | 43 | 90 | 35 | 68 |
| CSP-100 | 62 | 73 | 70 | 62 | 80 |
| PDIP-20 | 98 | 92 | 100 | 88 | 96 |
| QFN-20 | 0 | 21 | 20 | 8 | 10 |
| TQFP-144 | 60 | 63 | 64 | 70 | 70 |
| TSOP-50 | 62 | 73 | 86 | 77 | 80 |

Vibration Testing



| | Relative Ranking (Solder Alloy / Component Finish) | | | | | | | | | | |
|---------|--|-------------------|-------------------|-------------------|--------------------------|--------------------------|-------------------------------------|--|------------------------------------|---------------------|---------------|
| BGA-225 | Sn37Pb/ Sn37Pb | SAC305/ SAC405 | Sn37Pb/ SAC405 | SAC305/ Sn37Pb | Rwk Flux Only/ Sn37Pb | Rwk Flux Only/ SAC405 | Rwk Sn37Pb/SAC405 (SnPb Profile) | Rwk Sn37Pb/SAC405 (Pb-Free Profile) | SN100C/ SAC405 | | |
| | 1 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | | |
| CLCC-20 | Sn37Pb/ Sn37Pb | SAC305/ SAC305 | Sn37Pb/ SAC305 | SAC305/ Sn37Pb | SN100C/ SAC305 | | | | | | |
| | 1 | 3 | 2 | 3 | 3 | | | | | | |
| CSP-100 | Sn37Pb/ Sn37Pb | SAC305/ SAC105 | Sn37Pb/ SAC105 | SAC305/ Sn37Pb | Rwk Flux Only/ Sn37Pb | Rwk Flux Only/ SAC105 | Rwk Sn37Pb/SAC105 (SnPb Profile) | Rwk Sn37Pb/SAC105 (Pb-Free Profile) | SN100C/ SAC105 | | |
| | 1 | 1 | 1 | 2 | 1 | 2 | 1 | 3 | 1 | | |
| PDIP-20 | Sn37Pb/ SnPb | SN100C/ Sn | Sn37Pb/ NiPdAu | Rwk Sn37Pb/ Sn | Rwk Sn100C/ Sn | SN100C/ NiPdAu | | | | | |
| | 1 | 3 | 2 | 3 | 3 | 3 | | | | | |
| QFN-20 | Sn37Pb/ Sn37Pb | SAC305/ Sn | Sn37Pb/ Sn | SAC305/ Sn37Pb | SN100C/ Sn | | | | | | |
| | 1 | 2 | 1 | 1 | 2 | | | | | | |
| QFP-144 | Sn37Pb/ Sn | SAC305/ Sn | Sn37Pb/ NiPdAu | SAC305/ NiPdAu | Sn37Pb/ Sn37Pb Dip | SAC305/ SAC305 Dip | SN100C/ Sn | | | | |
| | 1 | 1 | 1 | 2 | 1 | 2 | 1 | | | | |
| TSOP-50 | Sn37Pb/ SnPb | Sn37Pb/ Sn | Sn37Pb/ SnBi | SAC305/ Sn | SAC305/ SnBi | SAC305/ SnPb | Rwk Sn37Pb/ SnPb | Rwk Sn37Pb/Sn (SnPb Profile) | Rwk Sn37Pb/Sn (Pb-free Profile) | Rwk SAC305/ SnBi | SN100C/ Sn |
| | 1 | 2* | 2* | 2* | 2* | 2 | 2 | 2* | 2* | 2 | 2 |

*Performance relative to Sn37Pb control may depend on orientation of the TSOP

: as good as or better than Sn37Pb control

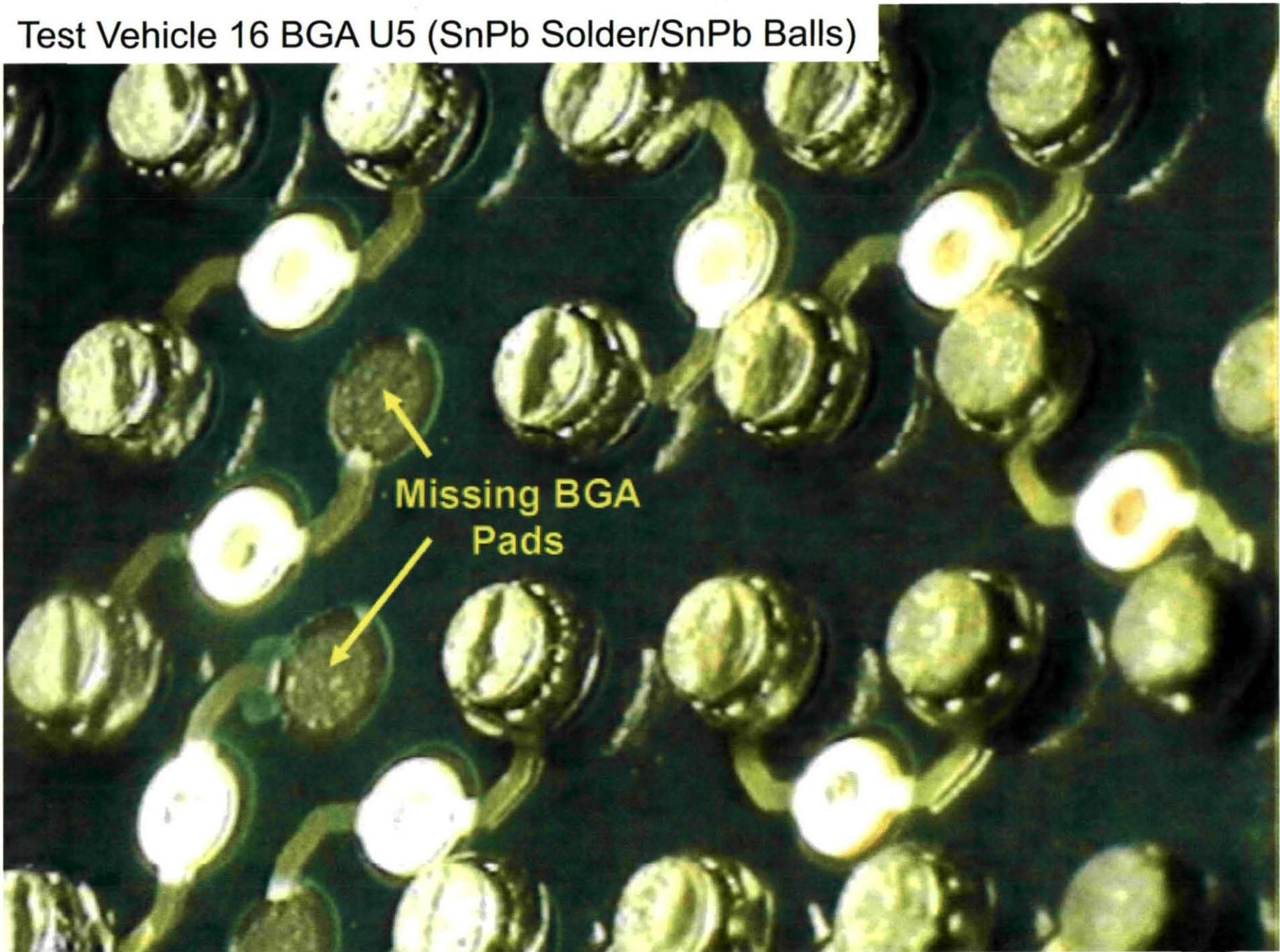
: worse than Sn37Pb control

: much worse than Sn37Pb control

Vibration Testing



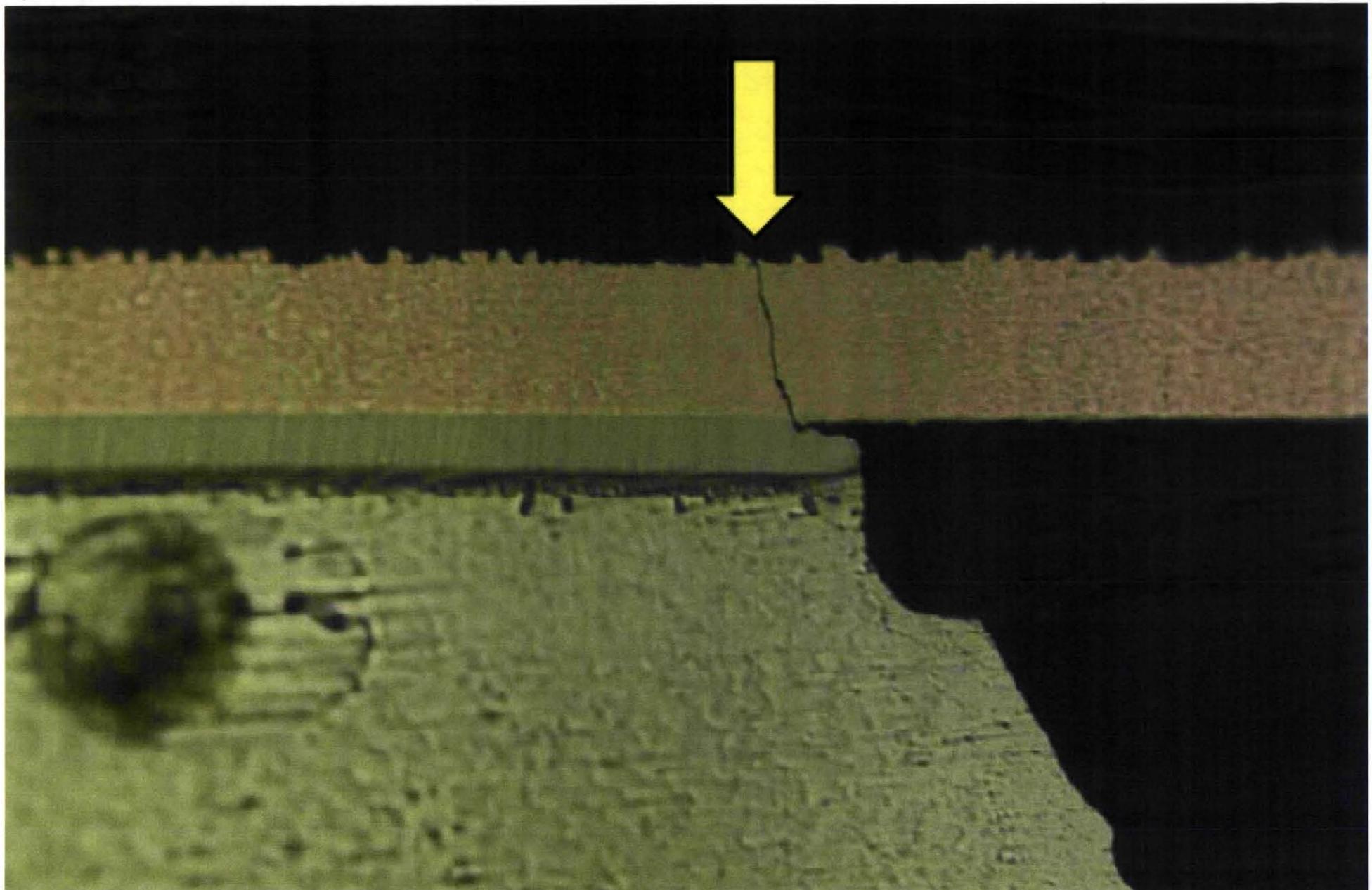
Test Vehicle 16 BGA U5 (SnPb Solder/SnPb Balls)



Vibration Testing



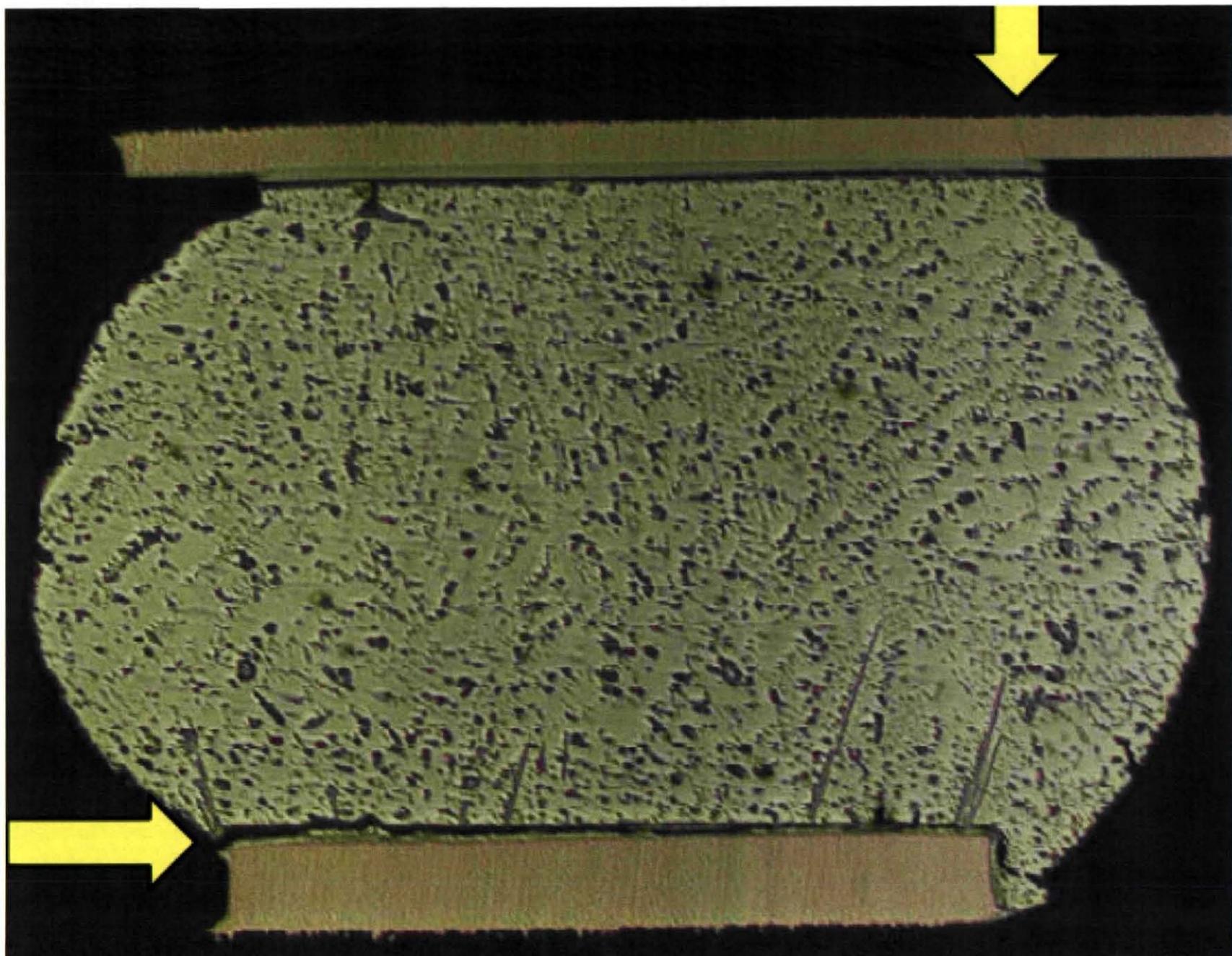
Test Vehicle 36 – Trace Crack on Component Side of BGA U21
(SAC305 Solder/SAC405 Balls)



Vibration Testing



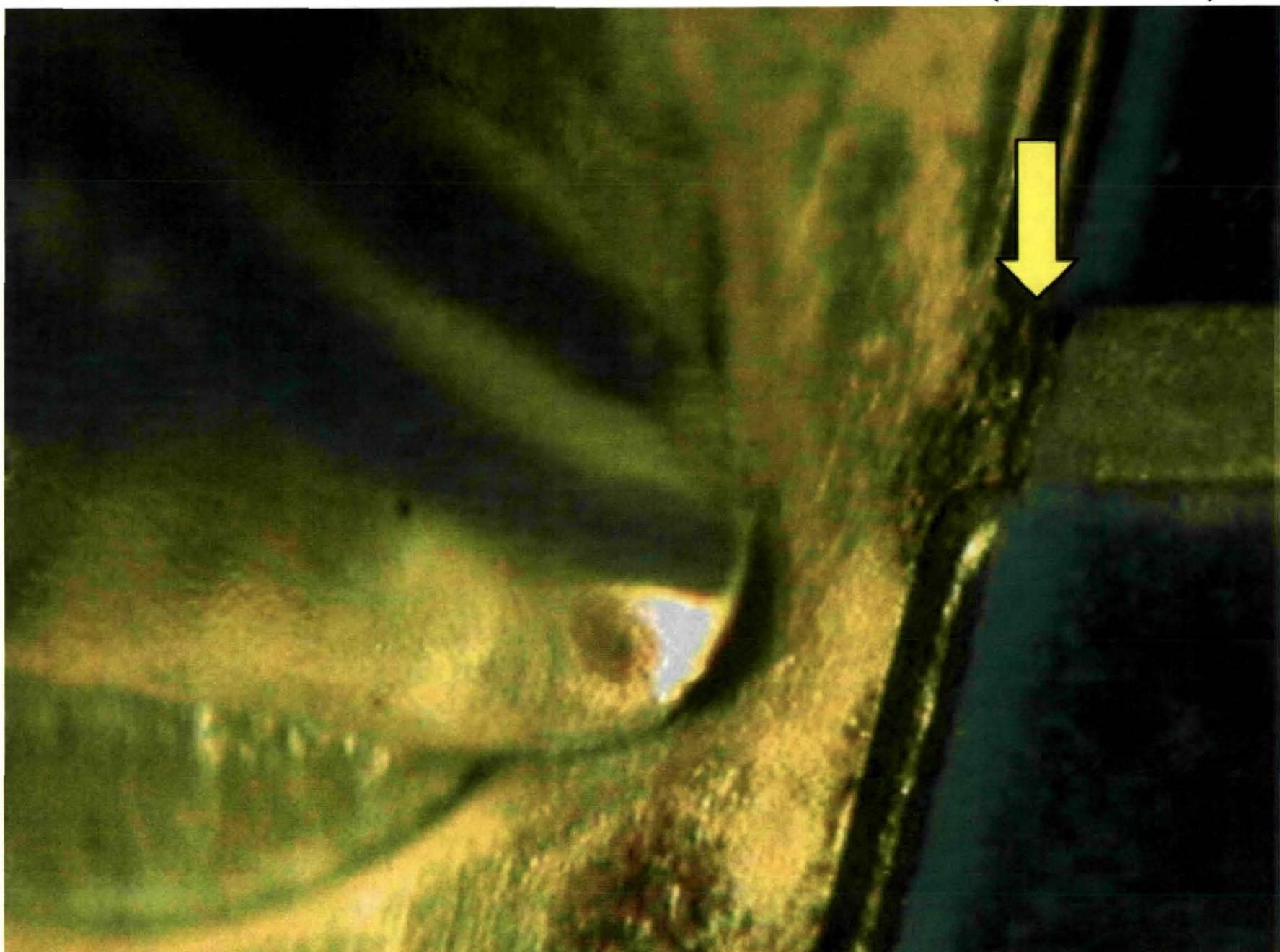
Test Vehicle 134 - Corner Ball of BGA U44 (SnPb Solder/SAC405 Balls)



Vibration Testing



Test Vehicle 112 – Cracked Trace at Corner of PDIP U38 (SN100C/Sn)



On-Going Failure Analysis

| Mechanical Shock Test Vehicles | | | |
|--------------------------------|--------------|--------------------|--|
| Failure Analysis Location | Test Vehicle | Component Location | Selection Criteria |
| Sandia | 153 | U43 | Look for cause of open |
| | 153 | U18 | Look for cause of early failure |
| | 153 | U6 | Examine solder mixing |
| | 153 | U11 | Look for cause of early failure with special focus on trace cracking |
| | 153 | U51 | Look for cause of early failure with special focus on trace cracking |
| NSWC Crane | 189 | U11 | Look for cause of early failure with special focus on trace cracking |
| | 189 | U51 | See if trace cracking is absent |
| | 190 | U44 | Examine solder mixing |
| | 190 | U56 | Look for cause of early failure |
| Drop Test Vehicles | | | |
| Failure Analysis Location | Test Vehicle | Component Location | Selection Criteria |
| Celestica | 144 | U4 | Early failure - Cycle 1 |
| | 25 | U4 | Early failure - Cycle 5 |
| | 27 | U5 | Early failure - Cycle 3 |
| | 29 | U6 | Early failure - Cycle 3 |
| | 26 | U56 | No failure - Comparison |
| | 77 | U5 | Early failure - Cycle 5 |
| | 187 | U4 | Early failure - Cycle 2 |
| | 92 | U5 | Early failure - Cycle 3 |
| | 59 | U6 | Early failure - Cycle 3 |
| | 58 | U56 | No failure - Comparison |
| | 159 | U4 | Early failure - Cycle 2 |
| | 159 | U44 | Early failure - Cycle 2 |
| | 159 | U6 | Early failure - Cycle 2 |
| | 159 | U56 | Early failure - Cycle 4 |

Upcoming Event

SMTAI 2010

- October 24 - 28, 2010
- Orlando, FL - Walt Disney World Swan and Dolphin Resort

NASA-DoD Presentations - October 28

- NASA-DoD Lead-Free Electronics Project – Update
- Drop Test Assessment of a Medium Complexity Assembly for High Reliability Applications
- NASA/DoD Lead-Free Electronics Project: Mechanical Shock Testing
- NASA-DoD Combined Environments Testing Results
- NASA/DoD Lead-Free Electronics Project: Vibration Testing
- NASA DoD -55°C to +125°C Thermal Cycle Test Results



Kurt Kessel
ITB, Inc.

NASA Technology Evaluation for Environmental Risk
Mitigation Principal Center (TEERM)
Kennedy Space Center, FL
Phone: 321-867-8480
E-Mail: kurt.r.kessel@nasa.gov
Website: www.teerm.nasa.gov

NASA-DoD Lead-Free Electronics Project:

http://www.teerm.nasa.gov/projects/NASA_DODLeadFreeElectronics_Proj2.html

JCAA/JGPP Lead-Free Solder Project

http://www.teerm.nasa.gov/projects/LeadFreeSolderTestingForHighReliability_Proj1.html

